

**A Complete Theoretical Framework
for Antarctica based ANITA
experiment and its Implication for
the ANITA Anomalous Events**

HEP Seminar

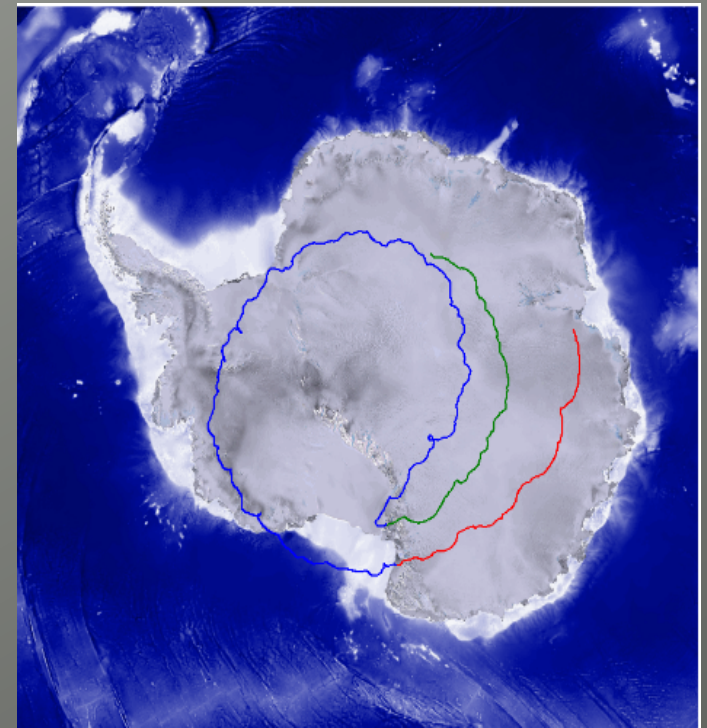
**The Service de Physique des Particules Élémentaires of the
Université Libre de Bruxelles (ULB)
Inter-University Institute for High Energies IIHE (ULB-VUB)
Belgium, Europe**

**Paramita Dasgupta, IIT Kanpur, India
24th April, 2020**

The ANITA Experiment

(**A**Ntarctic **I**mpulsive **T**ransient **A**ntenna)

NASA long-duration **balloon payload** with an array of radio antennas.



The balloon flying at a height 37Km above Antarctica, carries array of radio antennas to detect radio signals from Cosmic Neutrinos/UHECRs

Goals of ANITA Mission

- Search for high energy cosmogenic neutrinos by detecting their impulsive radio signals emitted via the **Askaryan effect** in the **Antarctic ice sheet** ← Primary goal
- ANITA is the First Experiment to Implement **Radio Technique** in the **EeV** Energy regime
(1 EeV = 10^{18} eV)
- UHECR induced radio emission in Air detected by balloon-borne radio antennas

Why Antarctica?

For EeV scale detection, we need huge detector

Lots of ice ~ 1 million Km³

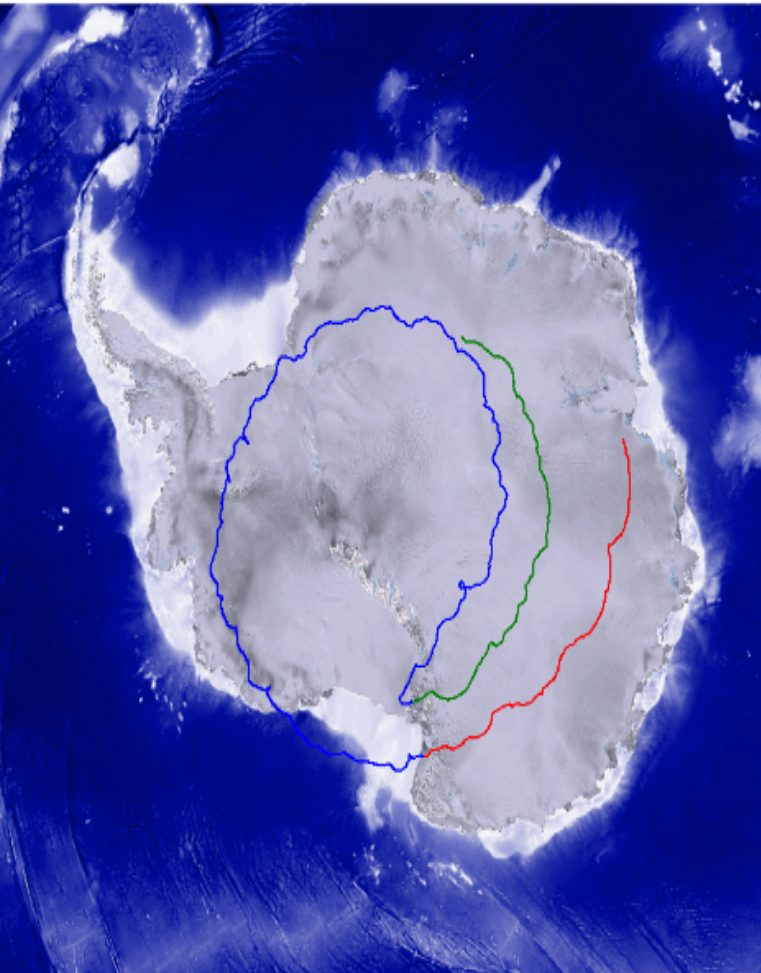
Coverage Radius ~ 700 Km

Detector at height ~ 37 Km

Ice has Excellent RF clarity

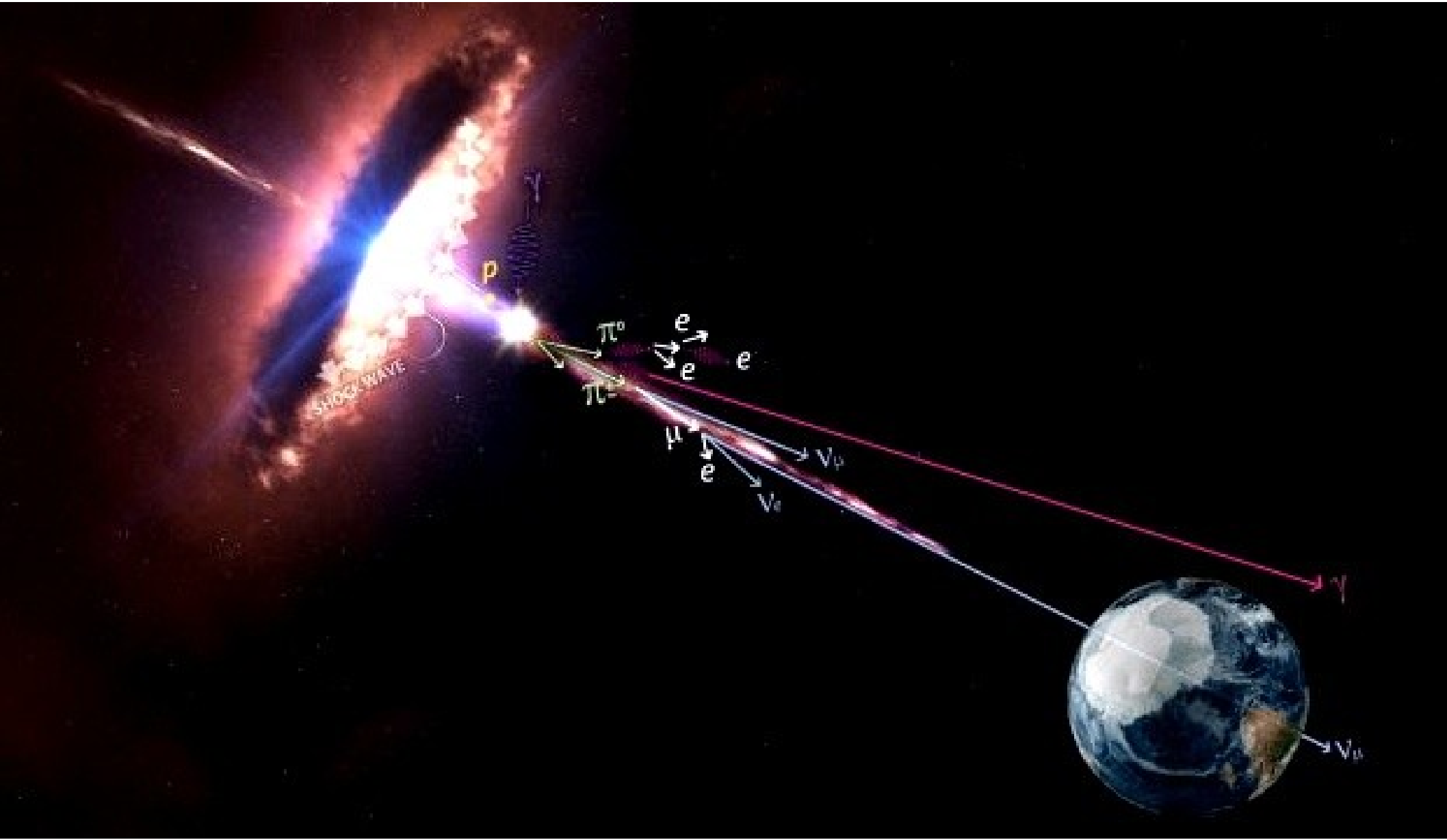
RF attenuation length: ~ 1km

Low Population, Less noise



IceCube (Energy ~ PeV), ARA, ARIANNA are other experiments in Antarctica

UHE Neutrinos: The Ideal Astronomical Messengers



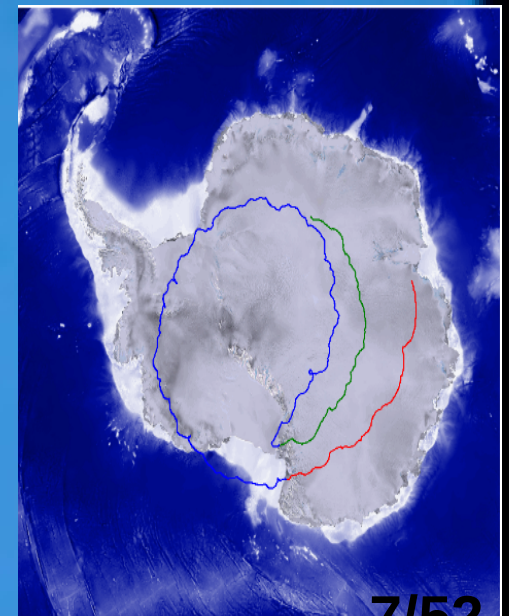
Experimentalists During the Launch of ANITA





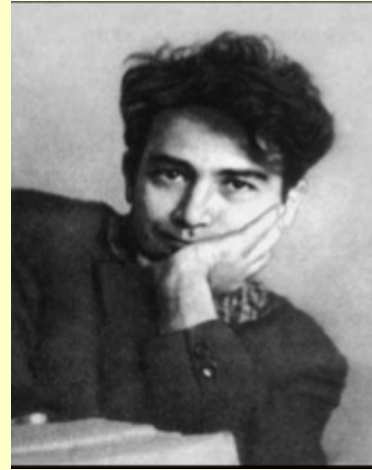


28-32 days at float



Primary Goal of ANITA :

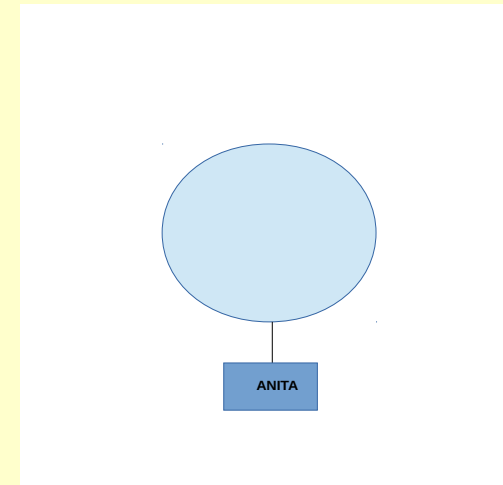
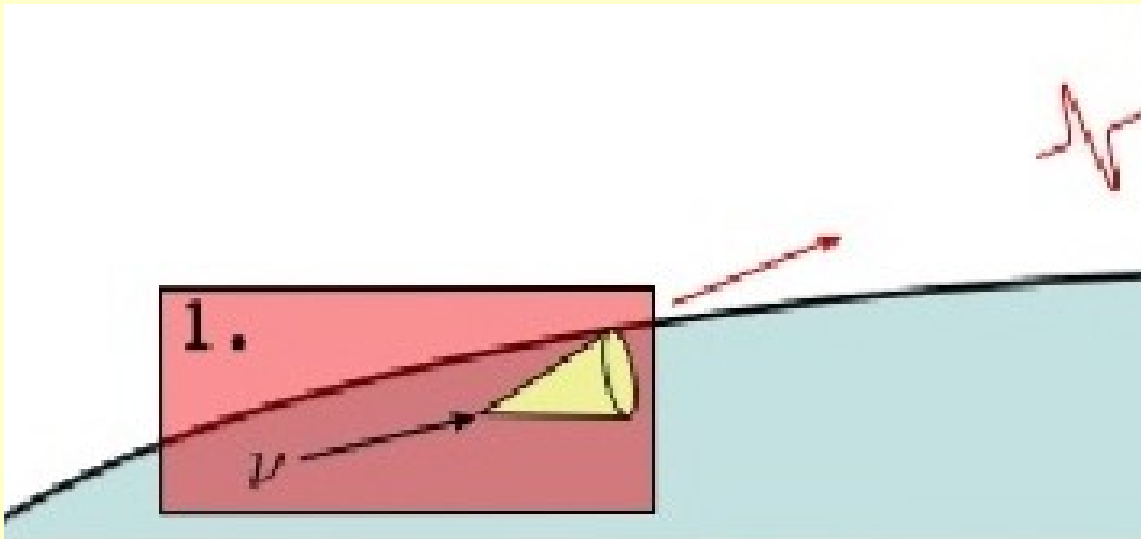
UHE ν Detection based on Askaryan Mechanism in dense medium (Antarctic ice)



Gurgen Askaryan

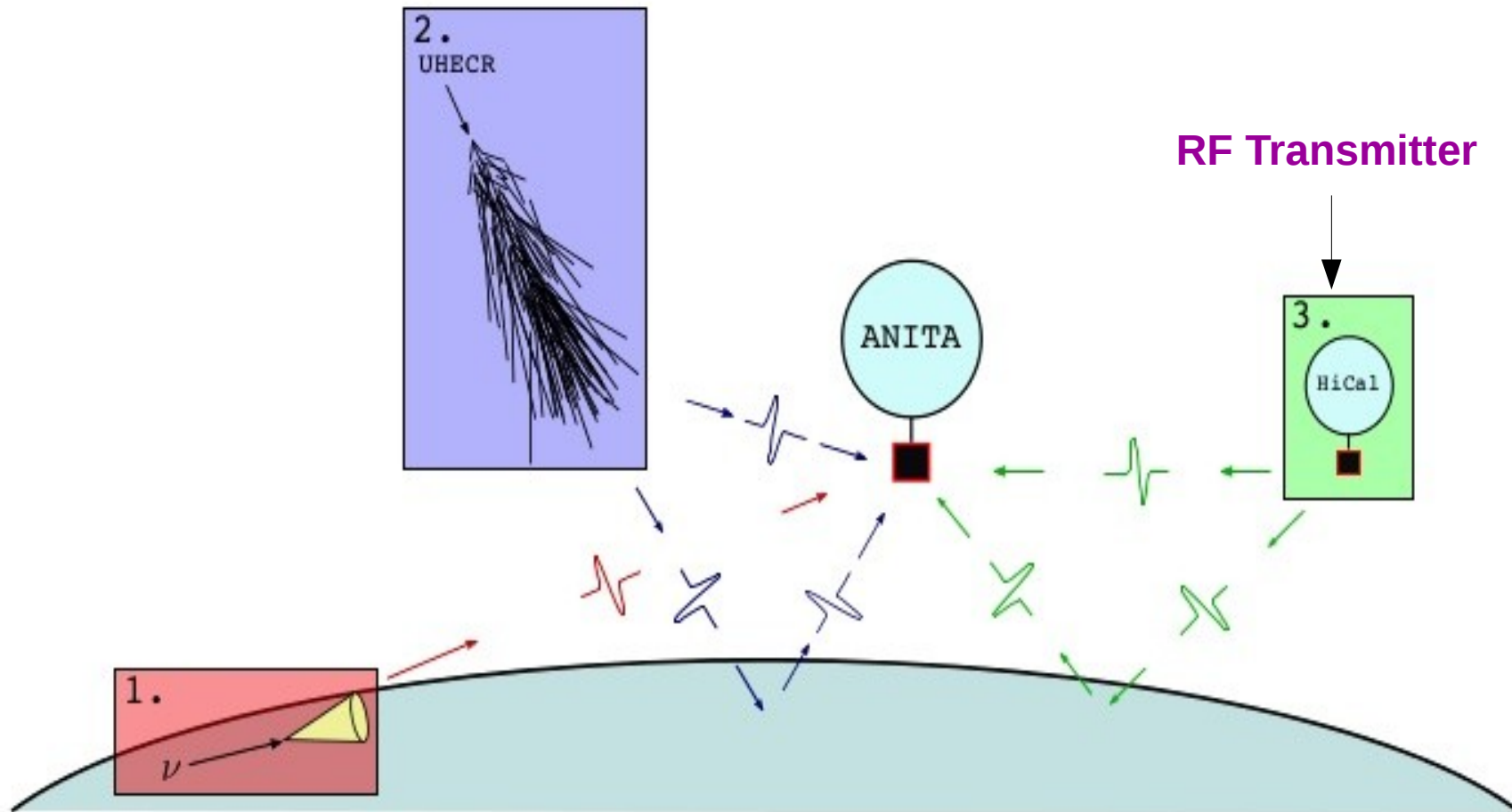
$\nu + \text{ice (H}_2\text{O)} \rightarrow \text{knock-on collisions} \rightarrow \text{excess } e^-$

Charge excess moving with velocity greater than the velocity of light in the traversed medium \rightarrow Cherenkov Radiation

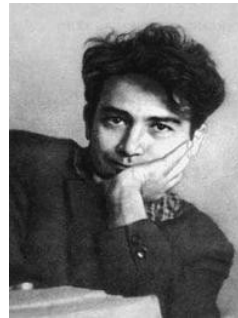


Working Principle of ANITA

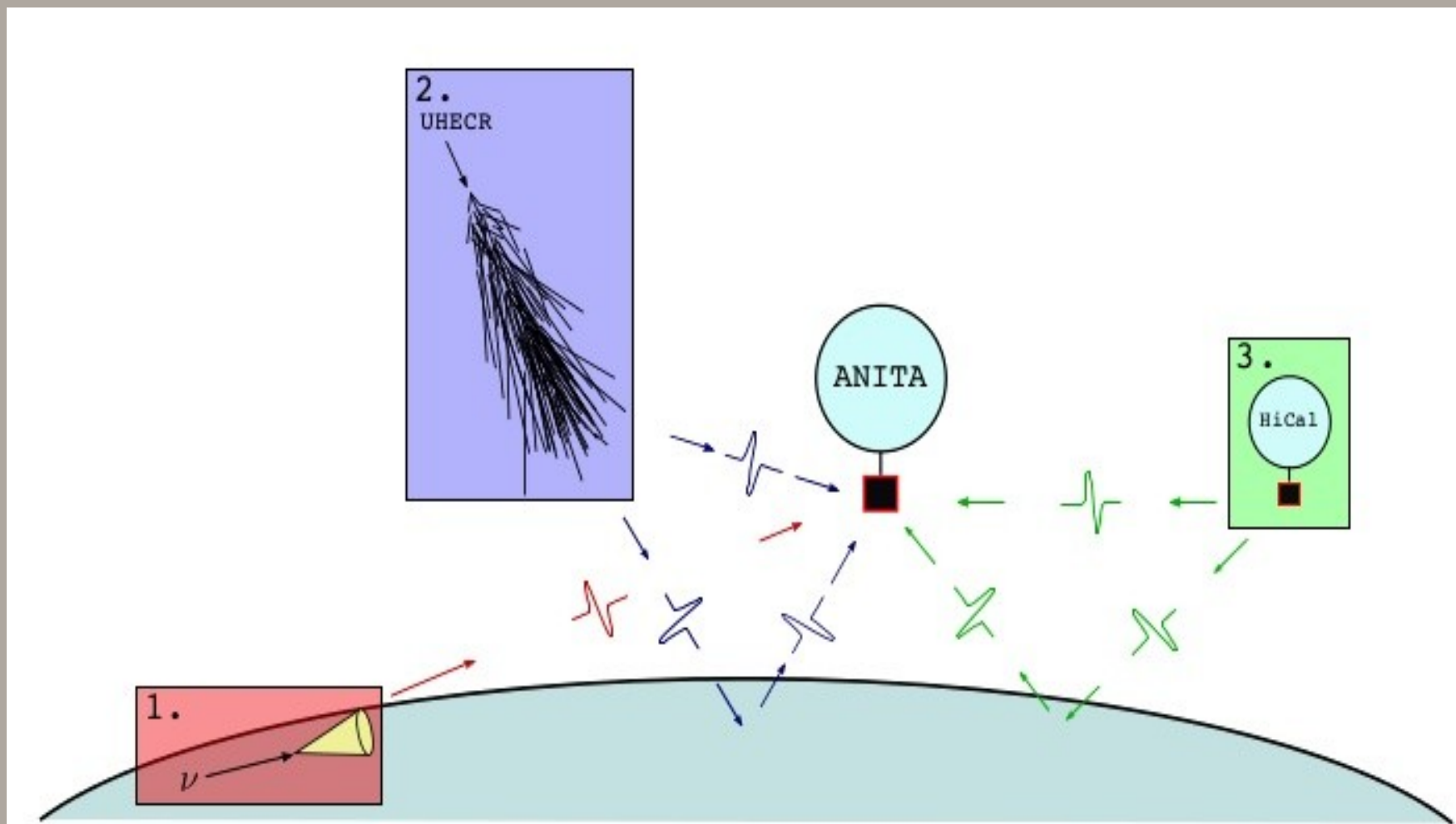
- Detect **UHE Neutrinos** via **Askaryan effect** in ice ← **Main Goal**
- **Coherent Geo-Synchrotron Radiation** at **Radio Frequencies** from highly relativistic **e^+e^- pair** gyrating in Earth's mag. field



Pavel Cherenkov

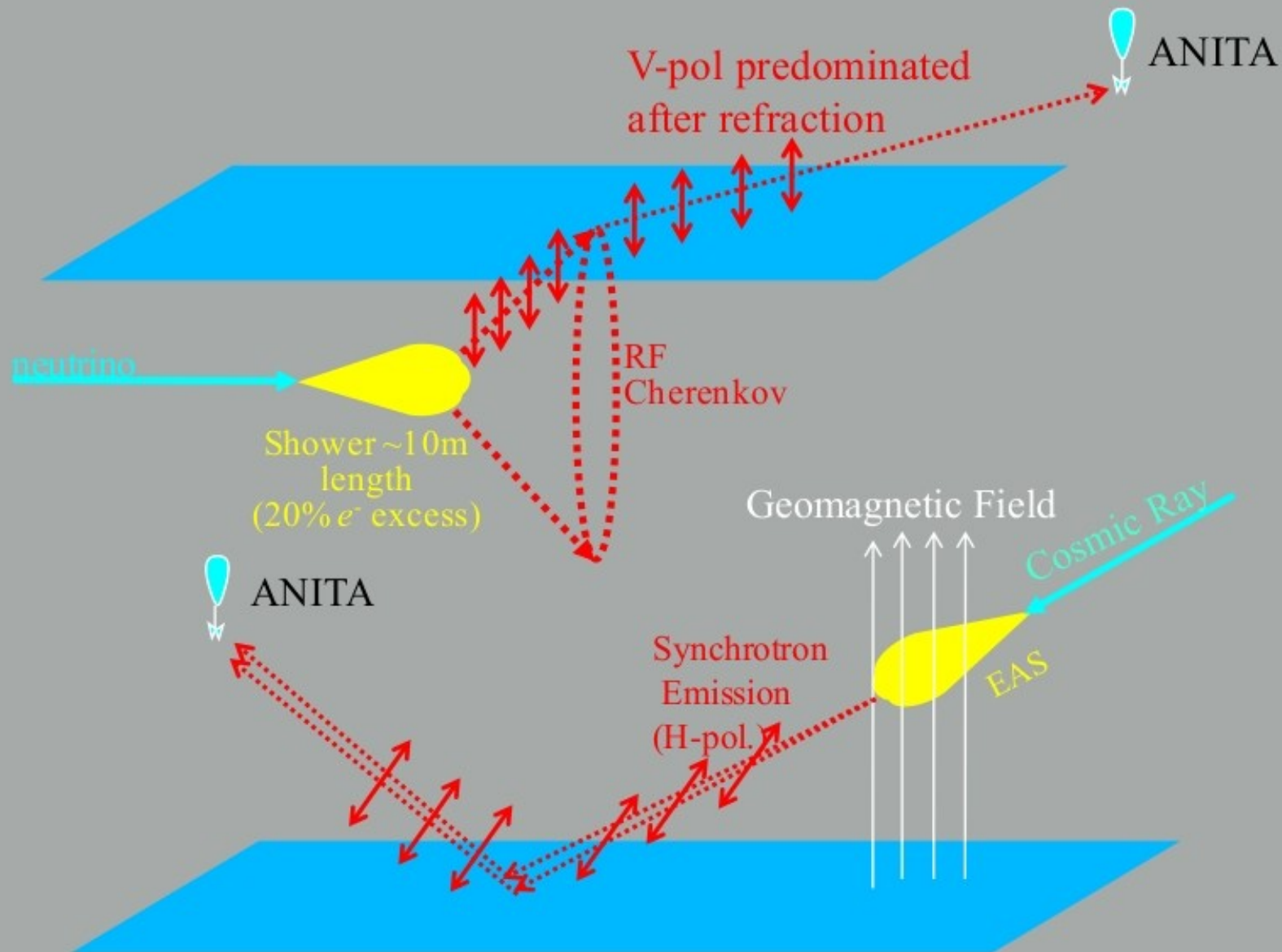


Gurgen Askaryan



**How to Distinguish between
Neutrino Induced signals
and
UHECR induced signals ?**

Neutrino Signal vs. Air Shower Signal



Diagrams courtesy of Jiwoo Nam

Contribution to ANITA Mission ?

Using First Principle Calculation

We developed

**“First Complete Theoretical
Framework” for ANITA**

&

**its successor Neutrino detection
experiments**

- **Development of First Complete & General theoretical framework for reflected RF signal simulation**

P. Dasgupta and P. Jain (Thesis supervisor)



- **Incorporated Antarctic Surface features & Curvature of Earth using First Principle Calculation**

- **Investigated the mystery of ANITA Anomalous Events**

- **Prof. David Besson** (at the Dept. Of Physics, Univ. of Kansas, USA) **& I investigated Antarctic subsurface Reflection and Transmission**

- **Extension of this formalism for in-ice** (such as RADAR, RNO-G) or under water neutrino detection

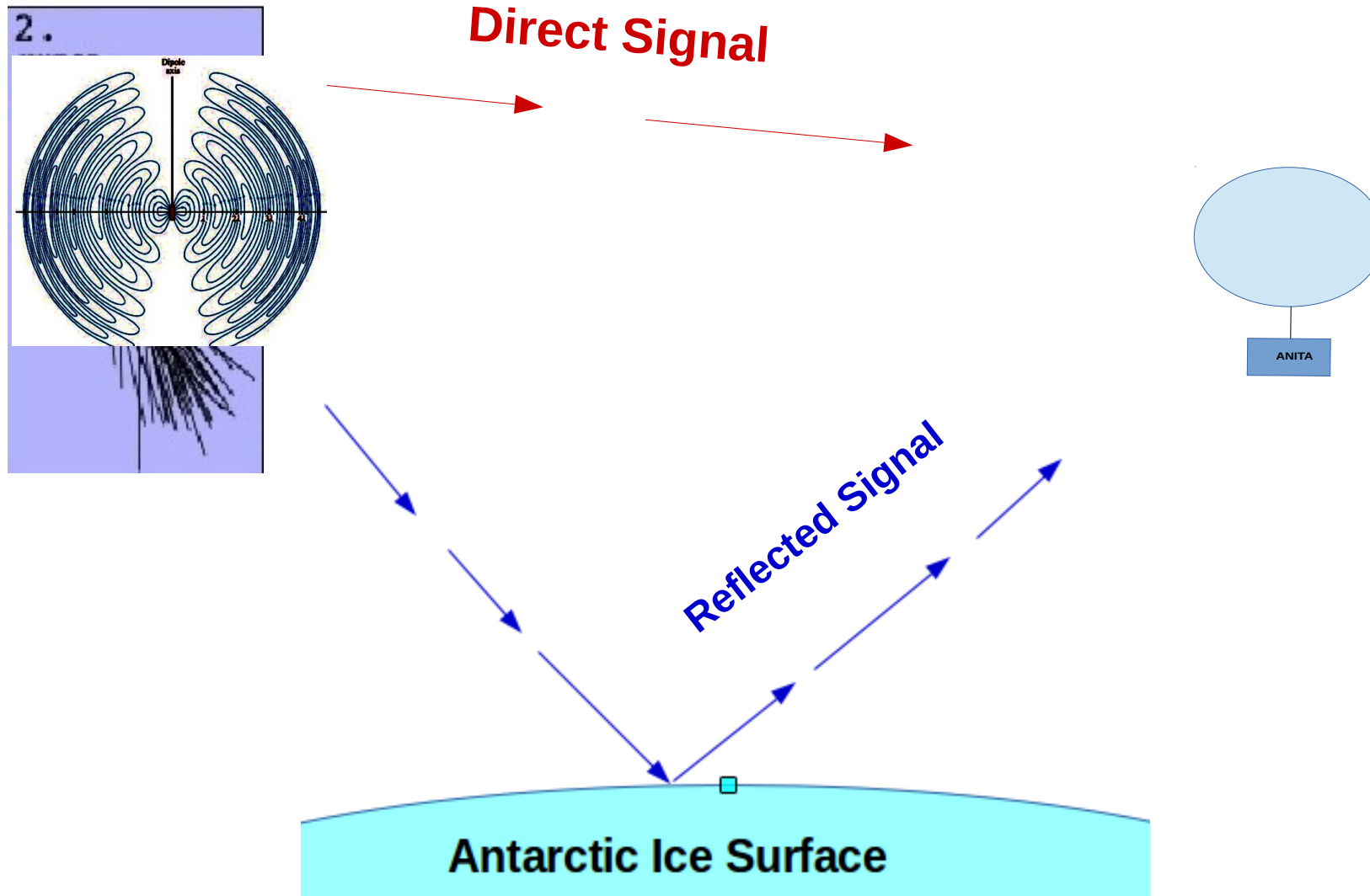


Development of Complete Theoretical Framework for NASA sponsored ANITA experiment

Decomposition of Spherical Waves into plane waves: Weyl Formalism (Year 1919)

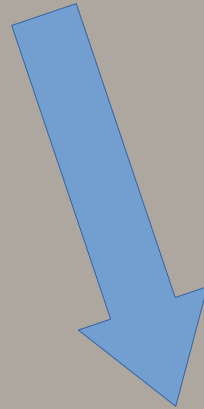
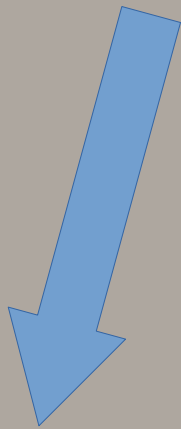
A dipole radiator on the z axis

- Extensive Air Shower (EAS)
- Geosynchrotron radiation (200- 650) MHz



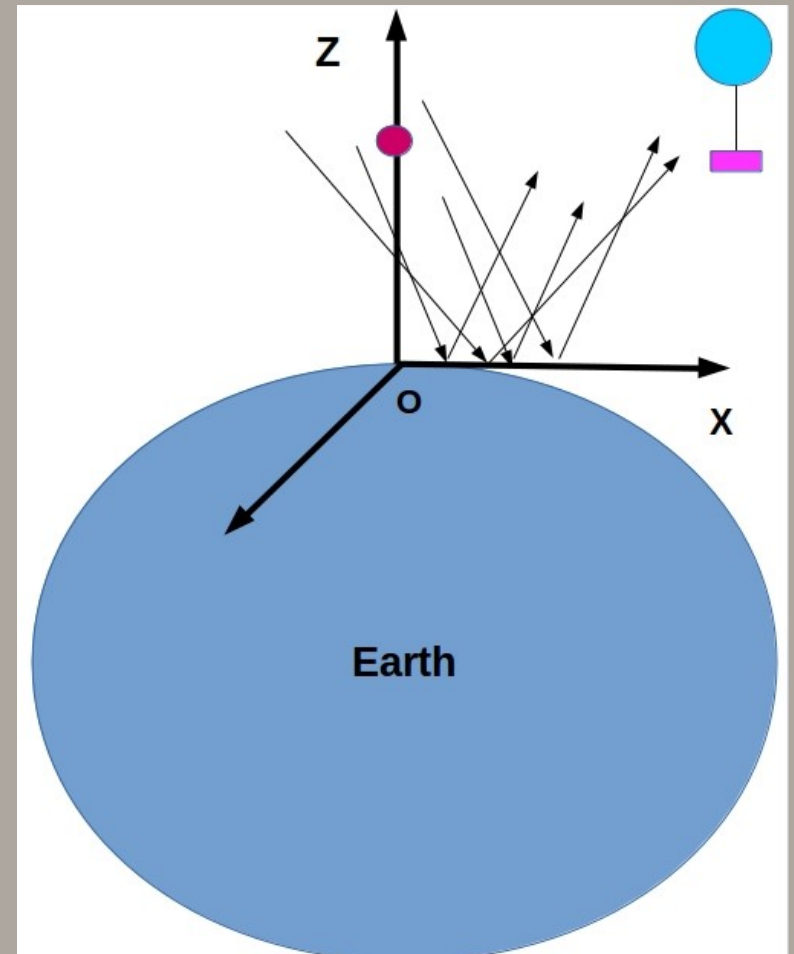
Start with the simplest case

Assume Earth Surface is FLAT



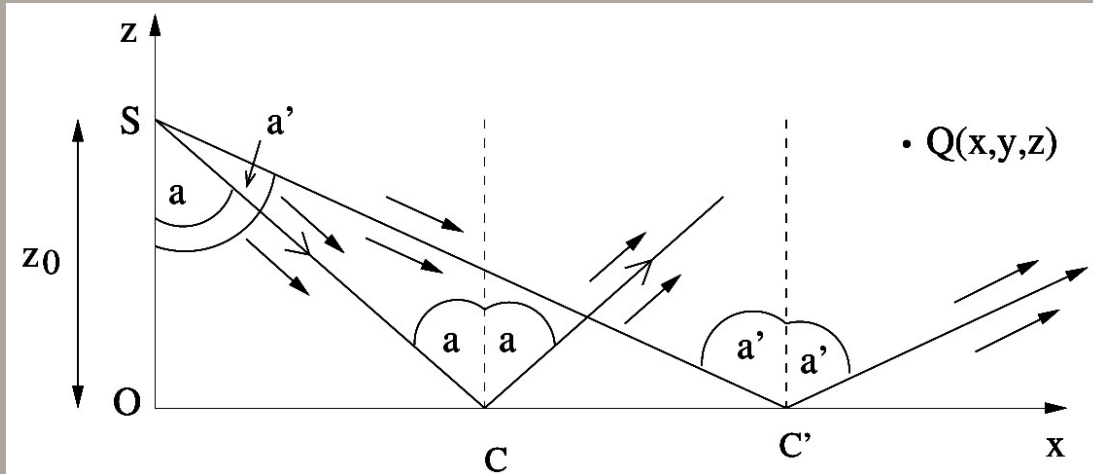
Flat + Smooth

Flat + Rough



Decomposition of Spherical Waves into plane waves: Weyl Formalism

Start with a Hertz dipole at $(0,0,z_0)$



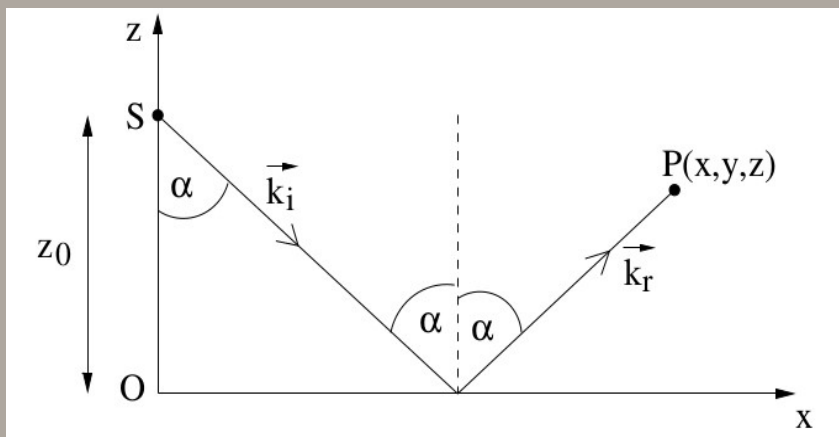
Hertz Potential (In Far Field $r \gg \lambda$)

$$\Pi_y(x, y, z) = \frac{e^{ikR}}{4\pi\epsilon R} + F_1(x, y, z)$$

Primary field

Due to reflection

$$\frac{e^{ikR}}{R} = \frac{ik}{2\pi} \int_0^{2\pi} \int_0^{\frac{\pi}{2}-i\infty} e^{ik[x \sin \alpha \cos \beta + y \sin \alpha \sin \beta + (z_0 - z) \cos \alpha]} \sin \alpha d\alpha d\beta$$



$$\vec{k}_I = k(\sin \alpha \cos \beta \hat{x} + \sin \alpha \sin \beta \hat{y} - \cos \alpha \hat{z})$$

$$\vec{k}_t = k_1[\sin \alpha_t \cos \beta_t \hat{x} + \sin \alpha_t \sin \beta_t \hat{y} - \cos \alpha_t \hat{z}]$$

Compute the Incident Field associated with each plane wave

$$\vec{E} = \vec{\nabla}(\vec{\nabla} \cdot \vec{\Pi}) + k^2 \vec{\Pi}$$

$$\vec{H} = \frac{k^2}{i\omega\mu} (\vec{\nabla} \times \vec{\Pi})$$

Electric and Magnetic field associated with each incident plane wave

$$\vec{E}_{\text{inc}} = \frac{ik^3}{8\epsilon\pi^2} \tilde{\Pi} [-\sin^2\alpha \cos\beta \sin\beta \hat{x} + (1 - \sin^2\alpha \sin^2\beta) \hat{y} + (\sin\alpha \sin\beta \cos\alpha) \hat{z}]$$

$$\vec{H}_{\text{inc}} = \frac{ik^2\omega}{8\pi^2} \tilde{\Pi} [\cos\alpha \hat{x} + (\cos\beta \sin\alpha) \hat{z}].$$

Decompose into s and p components

$$\vec{E}_{\text{inc}} = \vec{E}_{\text{inc}}^s + \vec{E}_{\text{inc}}^p$$

$$\vec{H}_{\text{inc}} = \vec{H}_{\text{inc}}^s + \vec{H}_{\text{inc}}^p$$

Reflection and Transmission: Flat Surface

- Reflected Field components $E_{\text{ref}}^s, E_{\text{ref}}^p, H_{\text{ref}}^s, H_{\text{ref}}^p$
- Transmitted Field Components $E_{\text{trans}}^s, E_{\text{trans}}^p, H_{\text{trans}}^s, H_{\text{trans}}^p$

$$\begin{aligned} E_{\text{ref}} &= E_{\text{ref}}^s + E_{\text{ref}}^p \\ E_{\text{trans}} &= E_{\text{trans}}^s + E_{\text{trans}}^p \end{aligned}$$

$$\begin{aligned} H_{\text{ref}} &= H_{\text{ref}}^s + H_{\text{ref}}^p \\ H_{\text{trans}} &= H_{\text{trans}}^s + H_{\text{trans}}^p \end{aligned}$$

Impose boundary conditions at $z=0$

$$f_r^s = \frac{k \cos \alpha - k_1 \cos \alpha_t}{k \cos \alpha + k_1 \cos \alpha_t}$$

$$f_t^s = \left(\frac{k}{k_1}\right)^2 \frac{2k_1 \cos \alpha}{k_1 \cos \alpha_t + k \cos \alpha}$$

$$f_r^p = \frac{k_1 \cos \alpha - k \cos \alpha_t}{k_1 \cos \alpha + k \cos \alpha_t}$$

$$f_t^p = \left(\frac{k}{k_1}\right)^2 \left(\frac{1}{\cos \alpha_t}\right) \frac{2k_1 \cos^2 \alpha}{k_1 \cos \alpha + k \cos \alpha_t}$$

Transmitted Field: Flat Reflecting Surface

$$E_{(trans),y} = \frac{ik_1^3}{8\epsilon_1\pi^2} \int_0^{2\pi} \int_0^{\frac{\pi}{2}-i\infty} \tilde{\Pi}_t(f_t^s \cos^2 \beta_t + f_t^p \cos^2 \alpha_t \sin^2 \beta_t) \sin \alpha d\alpha d\beta$$

**Transmitted Electric field component
perpendicular to the Plane of incidence
(H- Pol)**

Reflected Field (y component) for H-Pol : Flat Reflecting Surface

$$E_{(ref),y} = \frac{ik^3}{8\epsilon\pi^2} \int_0^{2\pi} \int_0^{\frac{\pi}{2}-i\infty} \tilde{\Pi}_{ref} (f_r^s \cos^2 \beta - f_r^p \cos^2 \alpha \sin^2 \beta) \sin \alpha d\alpha d\beta$$

Electric field component perpendicular to Plane of incidence (H- Pol)

Compute this Integral for different Elevation Angles in the Frequency range (200-650) MHz

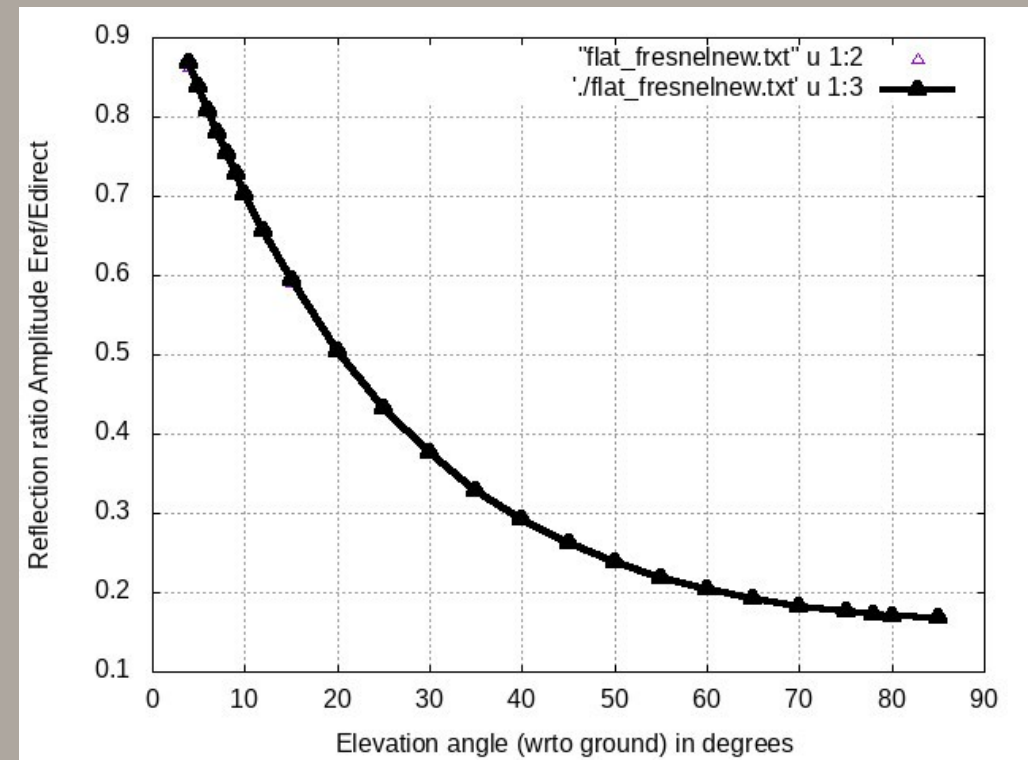
Also change R.I of ice from 1.25 to 1.75

Compare the simulated field Ref/Direct amplitude with Fresnel Coefficients

H-Pol (reflected/direct) amplitude Ratio: Flat Surface calculation using our theoretical framework

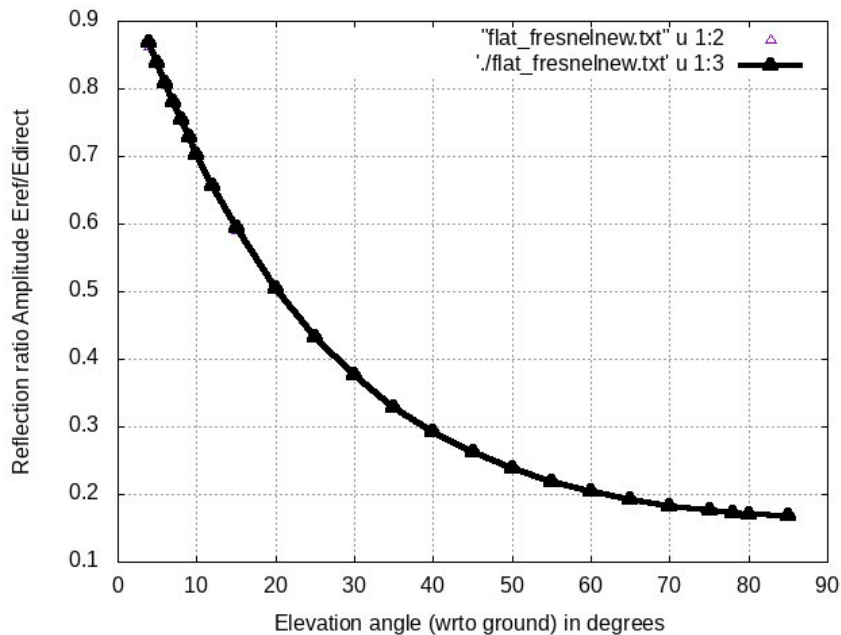
$$E_{(ref),y} = \frac{ik^3}{8\epsilon\pi^2} \int_0^{2\pi} \int_0^{\frac{\pi}{2}-i\infty} \tilde{\Pi}_{ref}(f_r^s \cos^2 \beta - f_r^p \cos^2 \alpha \sin^2 \beta) \sin \alpha d\alpha d\beta$$

| #angle(°) | #amp(flat) | #fresnel |
|-----------|------------|----------|
| 4 | 0.862801 | 0.867387 |
| 5 | 0.835699 | 0.837217 |
| 6 | 0.806814 | 0.808184 |
| 7 | 0.779242 | 0.780260 |
| 8 | 0.753162 | 0.753415 |
| 9 | 0.726390 | 0.727618 |
| 10 | 0.702397 | 0.702839 |
| 12 | 0.654847 | 0.656209 |
| 15 | 0.590581 | 0.593123 |
| 20 | 0.502614 | 0.504245 |
| 25 | 0.432435 | 0.432603 |
| 30 | 0.374581 | 0.375000 |
| 35 | 0.327991 | 0.328724 |
| 40 | 0.290877 | 0.291543 |
| 45 | 0.261001 | 0.261666 |
| 50 | 0.237114 | 0.237675 |
| 55 | 0.216842 | 0.218464 |
| 60 | 0.202191 | 0.203177 |
| 65 | 0.190783 | 0.191156 |
| 70 | 0.180672 | 0.181906 |
| 75 | 0.174257 | 0.175055 |
| 78 | 0.171902 | 0.171982 |
| 80 | 0.168961 | 0.170338 |
| 85 | 0.167334 | 0.167576 |



This framework works perfectly for a flat dielectric medium

Our result matches with **Fresnel Reflection and Transmission coefficients**

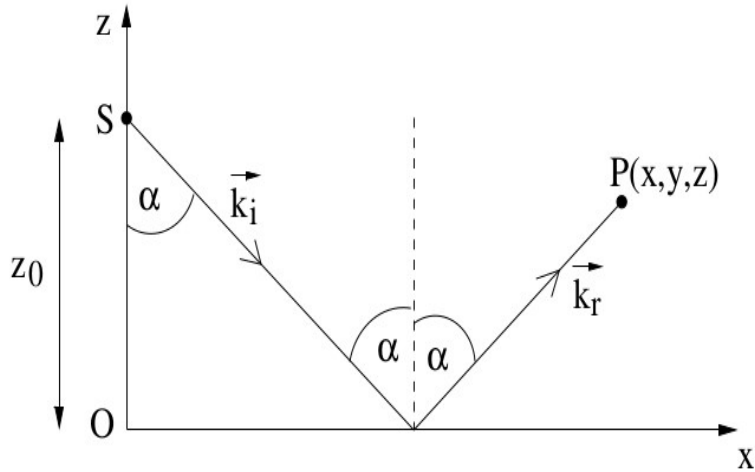


Now the realistic case of
Spherical +Uneven Earth Surface

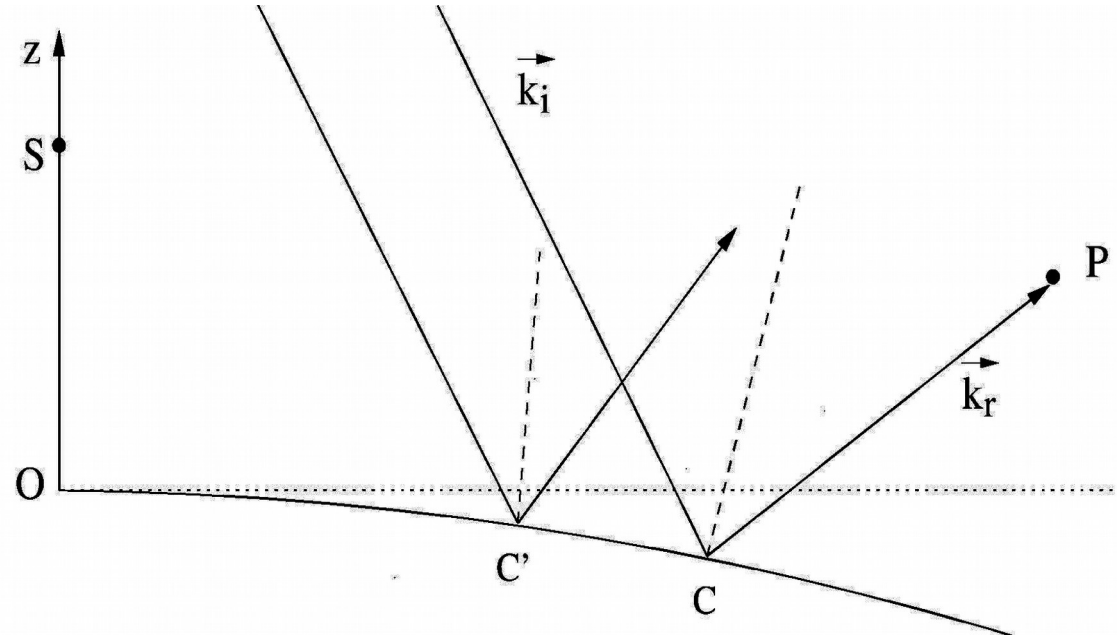
Complexity starts from here

A Rigorous Formalism to study the Radio Signals Reflecting off a **Spherical Surface**

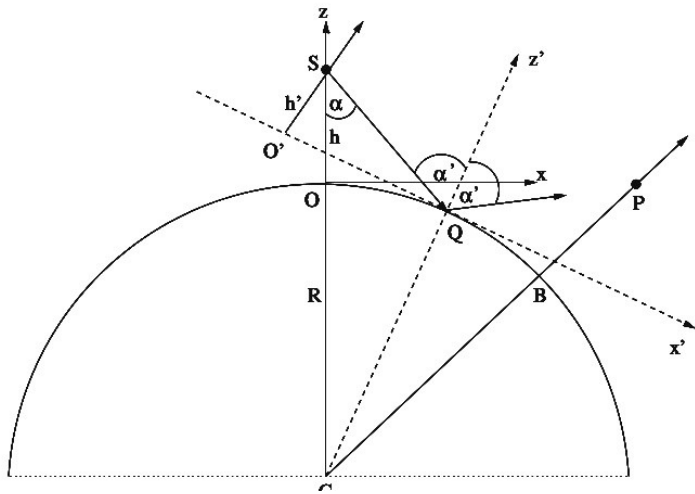
Flat Earth Surface



Spherical Earth Surface



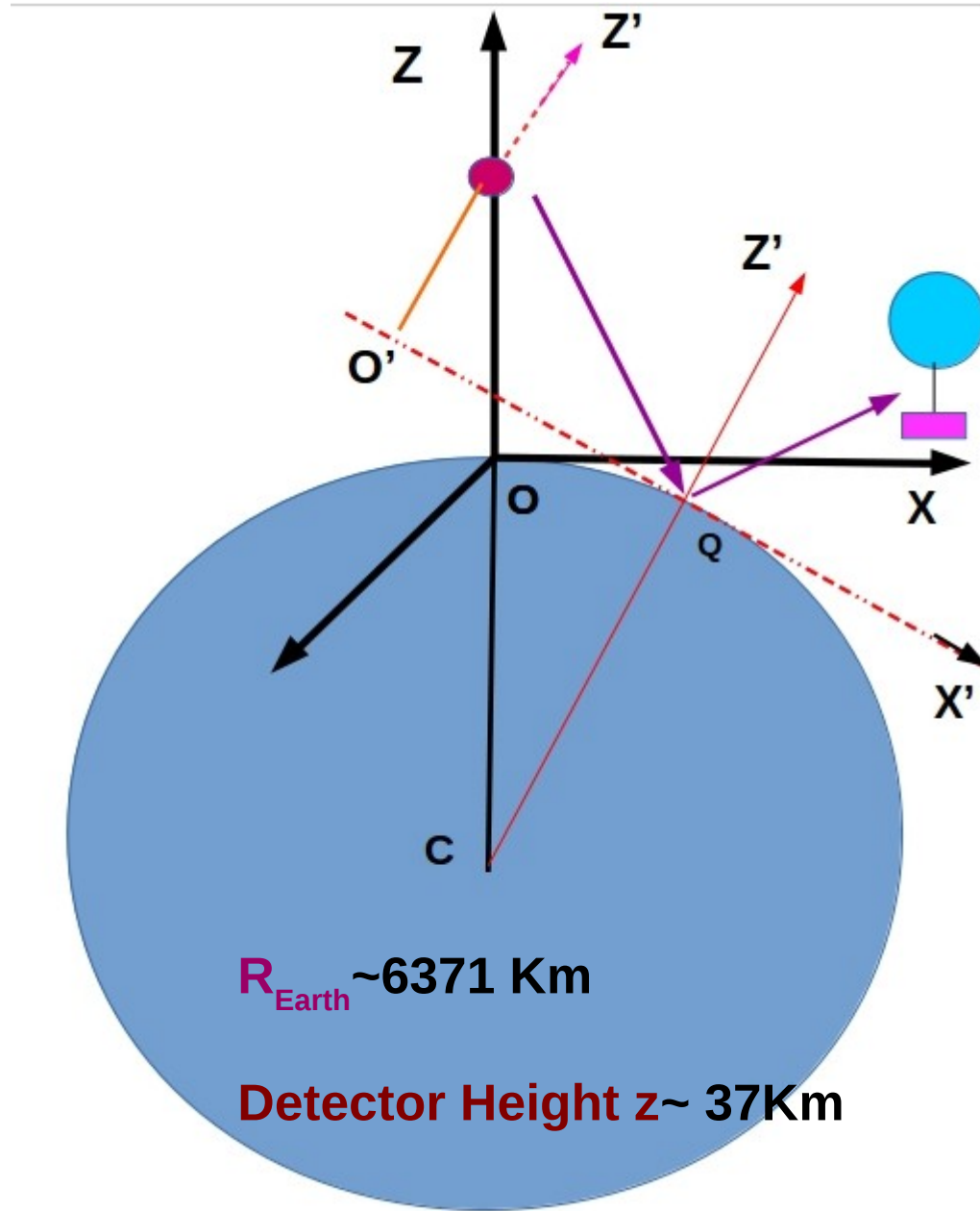
- We extend our Formalism for a Spherical Reflecting Surface
- We do not make any approximation
- Surface topography data for Roughness Model



For each plane wave with angle alpha and beta we need to find the rotation matrix to transform the coordinate system from x-y-z to x'-y'-z'

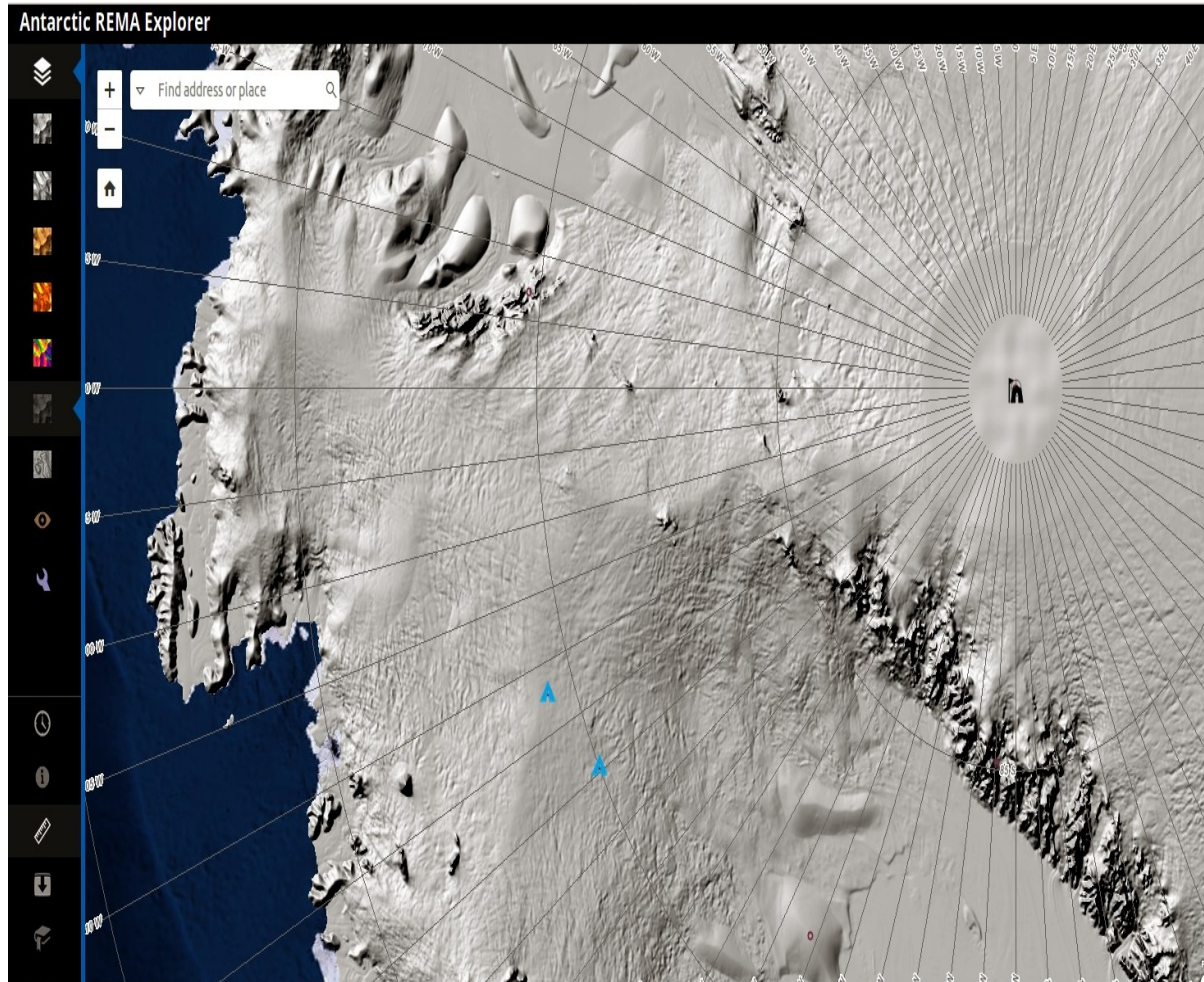
$$Rot = \begin{pmatrix} \cos(\alpha' - \alpha) \cos \beta & \cos(\alpha' - \alpha) \sin \beta & -\sin(\alpha' - \alpha) \\ -\sin \beta & \cos \beta & 0 \\ \sin(\alpha' - \alpha) \cos \beta & \sin(\alpha' - \alpha) \sin \beta & \cos(\alpha' - \alpha) \end{pmatrix}$$

We then translate the coordinate system to change o to o'



Antarctic Surface Topography from The Reference Elevation Model of Antarctica (REMA)

We receive this data from National Geospatial-Intelligence Agency
(NGA), USA



Antarctic Surface



Reflection and Transmission: Spherical Surface

• Reflected Field components $E'_{\text{ref}}^{(s)}$, $E'_{\text{ref}}^{(p)}$ & $H'_{\text{ref}}^{(s)}$, $H'_{\text{ref}}^{(p)}$

• Transmitted Field Components $E'_{\text{trans}}^{(s)}$, $E'_{\text{trans}}^{(p)}$ & $H'_{\text{trans}}^{(s)}$, $H'_{\text{trans}}^{(p)}$

$$E'_{\text{ref}} = E'_{\text{ref}}^{(s)} + E'_{\text{ref}}^{(p)}$$

$$E'_{\text{trans}} = E'_{\text{trans}}^{(s)} + E'_{\text{trans}}^{(p)}$$

$$H'_{\text{ref}} = H'_{\text{ref}}^{(s)} + H'_{\text{ref}}^{(p)}$$

$$H'_{\text{trans}} = H'_{\text{trans}}^{(s)} + H'_{\text{trans}}^{(p)}$$

Impose boundary conditions at $z' = 0$

$$f_r^{s} = \frac{k \cos \alpha' - k_1 \cos \alpha'_t}{k \cos \alpha' + k_1 \cos \alpha'_t},$$

$$f_t^{s} = \left(\frac{k}{k_1}\right)^2 \frac{2k_1 \cos \alpha'}{k \cos \alpha' + k_1 \cos \alpha'_t}.$$

$$f_r^{p} = \frac{k_1 \cos \alpha' - k \cos \alpha'_t}{k_1 \cos \alpha' + k \cos \alpha'_t}$$

$$f_t^{p} = \left(\frac{k}{k_1}\right)^2 \left(\frac{1}{\cos \alpha'_t}\right) \frac{2k_1 \cos \alpha \cos \alpha'}{k_1 \cos \alpha' + k \cos \alpha'_t}.$$

Antarctic Surface Roughness Model by Peter Gorham

Gorham's Roughness Model is an average roughness model

We started with simple model to compute reflected fields



L is the radius we compute around the specular angle θ_z

For $L_0 = 150$ m, $\sigma_h(L) = 0.041$ m

$H =$ Hurst Parameter $= 0.65$


$$\sigma_h(L) = \sigma_h(L_0) \left(\frac{L}{L_0} \right)^H$$

$$F(k, \rho, \theta) = \exp[-2k^2 \sigma_h(\rho_{\perp})^2 \cos^2 \theta_z]$$

k (wave number) is dependent on the Frequency of Incoming wave

After Computing Electric and Magnetic fields in $x'-y'z'$

We transform back to the original ($x-y-z$) coordinate system by inverse rotation



$\vec{E}_{\text{ref}} = \text{Rot}^{-1} \cdot \vec{E}'_{\text{ref}}$

&

$\vec{H}_{\text{ref}} = \text{Rot}^{-1} \cdot \vec{H}'_{\text{ref}}$

Reflected fields for Spherical + **Rough** Reflecting Surface

$$\exp(i[\vec{k}'_{\text{inc}} \cdot (\vec{r}'_s - \vec{h}') + \vec{k}'_{\text{ref}} \cdot (\vec{r}' - \vec{r}'_s)])$$

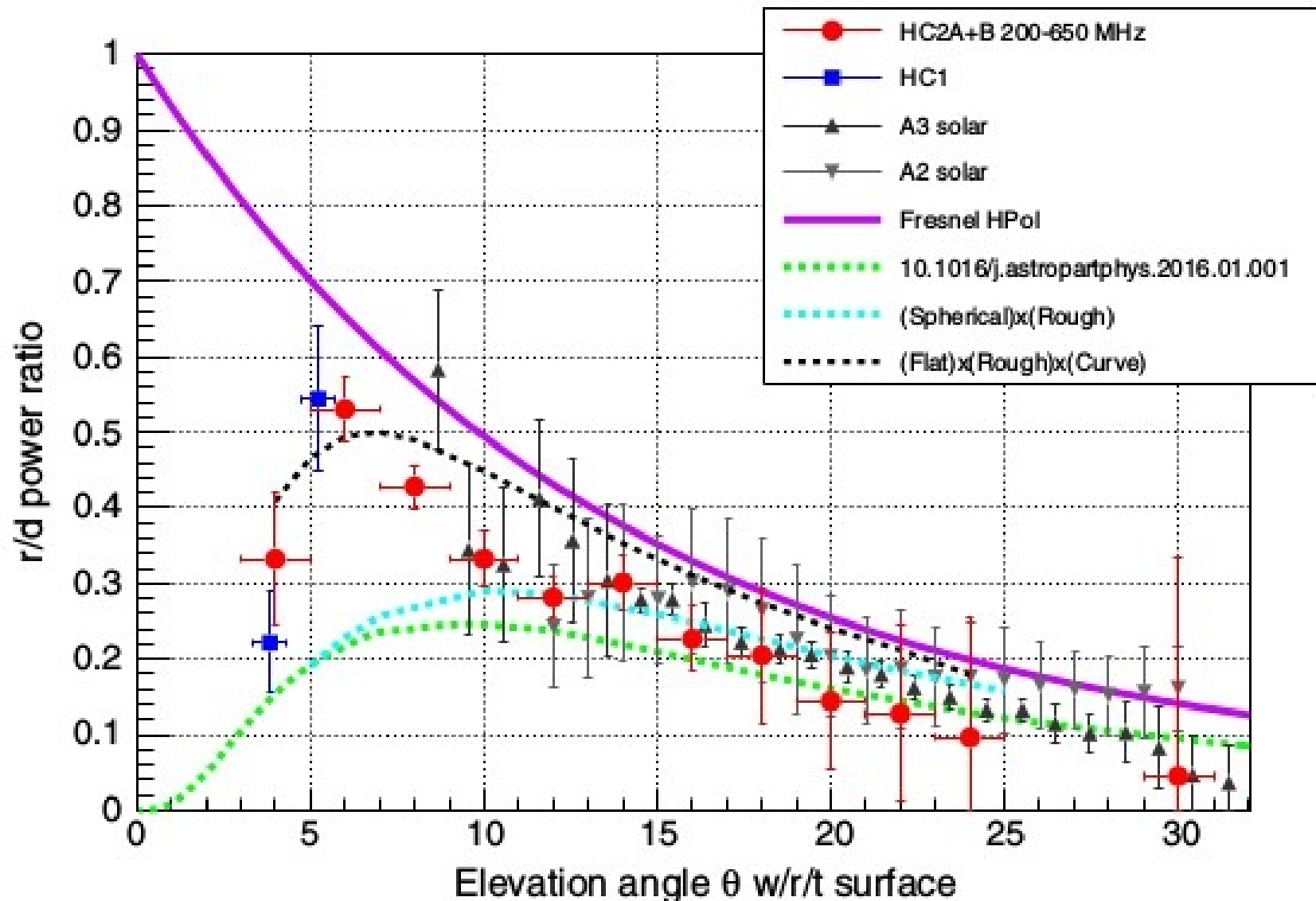
$$E_{\text{ref},y} = \frac{1}{2} \frac{ik^3}{8\epsilon\pi^2} \tilde{\Pi}_{S,r} F(k, \rho, \theta) [f_r'^s (1 + \cos 2\beta) - f_r'^p \cos \alpha \cos(2\alpha' - \alpha) (1 - \cos 2\beta)]$$

Integrating over $d\Omega$ gives Total E_{ref} (H-Pol)

Take Ratio with the amplitude of Direct pulse propagated from Dipole to Detector

Compare this amplitude ratio r/d with the HiCal Experimental data

r/d power ratio compared with HiCal data



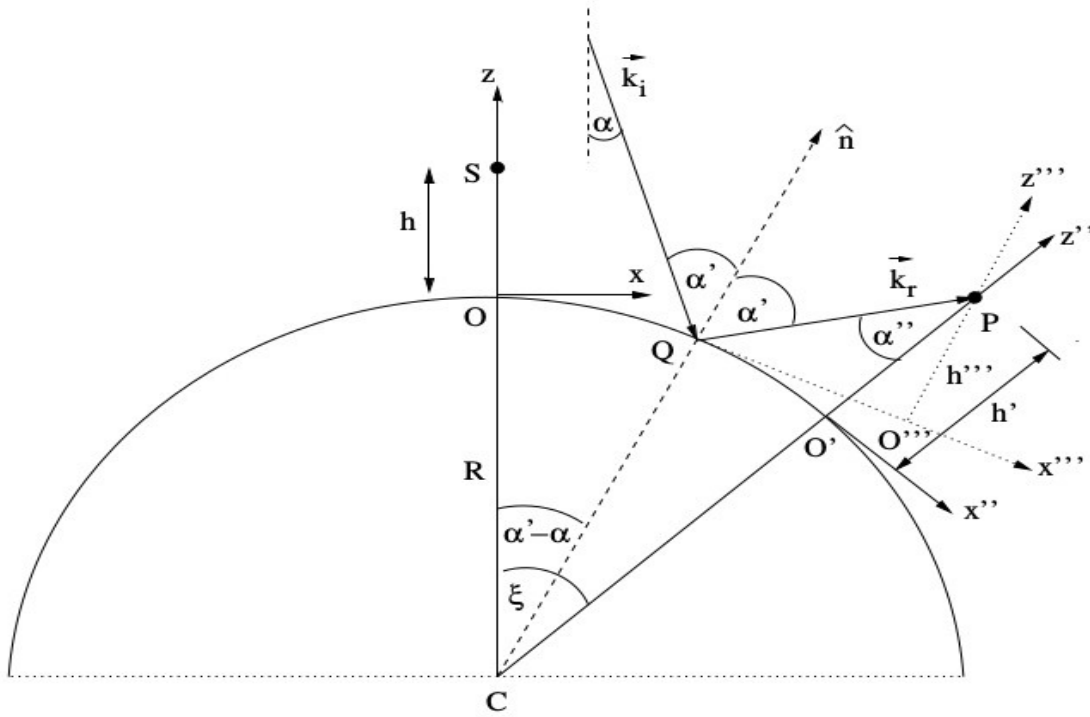
Testing our Framework

- We Compute Reflected H-Pol Fields and compared with HiCal-2 Data
- This Formalism works very well for elevation angle $>10^\circ$
- For elevation angle $< 10^\circ$ are off from HiCal-2 data
- Results shown in August 2018 in **Physical Review D. Volume 98, 042004**
- Refinement of the Framework is necessary to apply this model for all elevation angles applicable to ANITA payload”

Refinement of our theory

- Next, we developed a formalism called **“Local Plane Wave Approximation”** which is a modified version of our theory developed in *Physical Review D*, volume 98, 042004
- This theoretical development is currently under review in *Astroparticle Physics Journal* ([arXiv:1811.00900v2](https://arxiv.org/abs/1811.00900v2))

Refinement of Framework : “Local Plane Wave Approximation”



$$Rot_1 = \begin{pmatrix} \cos \xi \cos \tilde{\beta} & \sin \tilde{\beta} & -\sin \xi \cos \tilde{\beta} \\ -\cos \xi \sin \tilde{\beta} & \cos \tilde{\beta} & \sin \xi \sin \tilde{\beta} \\ \sin \xi & 0 & \cos \xi \end{pmatrix}$$

By **Rotating** the coordinate system and subsequent **translation** we make sure \mathbf{k}'''_{inc} , \mathbf{k}'''_{ref} & local normal lie **in the same plane**

$$\begin{aligned} \vec{E}_i''' &= R_{y'}(\psi) \vec{E}_i' \\ &= \frac{ik^3}{8\epsilon\pi^2} \tilde{\Pi}_{S,i} [(\sin \tilde{\beta} \cos^2 \tilde{\alpha} \cos \psi + \sin \alpha \cos \tilde{\alpha} \sin \beta \sin \psi) \hat{x}''' + \cos \tilde{\beta} \hat{y}''' \\ &\quad + (\sin \alpha \cos \tilde{\alpha} \sin \beta \cos \psi - \cos^2 \tilde{\alpha} \sin \tilde{\beta} \sin \psi) \hat{z}'''] \end{aligned}$$

$$\begin{aligned} \vec{H}_i''' &= R_{y'}(\psi) \vec{H}_i' \\ &= \frac{ik^2\omega}{8\pi^2} \tilde{\Pi}_{S,i} [\cos \tilde{\beta} \cos(\tilde{\alpha} - \psi) \hat{x}''' - \cos \tilde{\alpha} \sin \tilde{\beta} \hat{y}''' \\ &\quad + \cos \tilde{\beta} \sin(\tilde{\alpha} - \psi) \hat{z}'''] \end{aligned}$$

Reflection and Transmission: Spherical Surface with Local Plane Wave Analysis

- Reflected Field components $\mathbf{E}'''(s)_{\text{ref}}$, $\mathbf{E}'''(p)_{\text{ref}}$ & $\mathbf{H}'''(s)_{\text{ref}}$, $\mathbf{H}'''(p)_{\text{ref}}$
- Transmitted Field components $\mathbf{E}'''(s)_{\text{trans}}$, $\mathbf{E}'''(p)_{\text{trans}}$ & $\mathbf{H}'''(s)_{\text{trans}}$, $\mathbf{H}'''(p)_{\text{trans}}$

$$\mathbf{E}'''_{\text{ref}} = \mathbf{E}'''(s)_{\text{ref}} + \mathbf{E}'''(p)_{\text{ref}}$$

$$\mathbf{E}'''_{\text{trans}} = \mathbf{E}'''(s)_{\text{trans}} + \mathbf{E}'''(p)_{\text{trans}}$$

$$\mathbf{H}'''_{\text{ref}} = \mathbf{H}'''(s)_{\text{ref}} + \mathbf{H}'''(p)_{\text{ref}}$$

$$\mathbf{H}'''_{\text{trans}} = \mathbf{H}'''(s)_{\text{trans}} + \mathbf{H}'''(p)_{\text{trans}}$$

Impose boundary conditions at $z=0$

$$f_r^{(s)} = \frac{k \cos(\tilde{\alpha} - \psi) - k_1 \cos(\tilde{\alpha}_t - \psi)}{k \cos(\tilde{\alpha} - \psi) + k_1 \cos(\tilde{\alpha}_t - \psi)},$$

$$f_r^{(p)} = \frac{k_1 \cos(\tilde{\alpha} - \psi) - k \cos(\tilde{\alpha}_t - \psi)}{k_1 \cos(\tilde{\alpha} - \psi) + k \cos(\tilde{\alpha}_t - \psi)},$$

$$f_t^{(s)} = \left(\frac{k}{k_1}\right)^2 \frac{2k_1 \cos(\tilde{\alpha} - \psi)}{k \cos(\tilde{\alpha} - \psi) + k_1 \cos(\tilde{\alpha}_t - \psi)}$$

$$f_t^{(p)} = \left(\frac{k}{k_1}\right)^2 \left(\frac{1}{\cos \tilde{\alpha}_t}\right) \frac{2k_1 \cos(\tilde{\alpha} - \psi) \cos \tilde{\alpha}}{k_1 \cos(\tilde{\alpha} - \psi) + k \cos(\tilde{\alpha}_t - \psi)}$$

Local Plane Wave Approximation: Electric and Magnetic Field (HPol & VPol)

Peter Gorham's roughness model

$$F(k, \rho, \theta) = \exp[-2k^2 \sigma_h(\rho_\perp)^2 \cos^2 \theta_z]$$

$$\sigma_h(L) = \sigma_h(L_0) \left(\frac{L}{L_0}\right)^H$$

Reflected fields for a **Spherical + Rough** Reflecting Surface

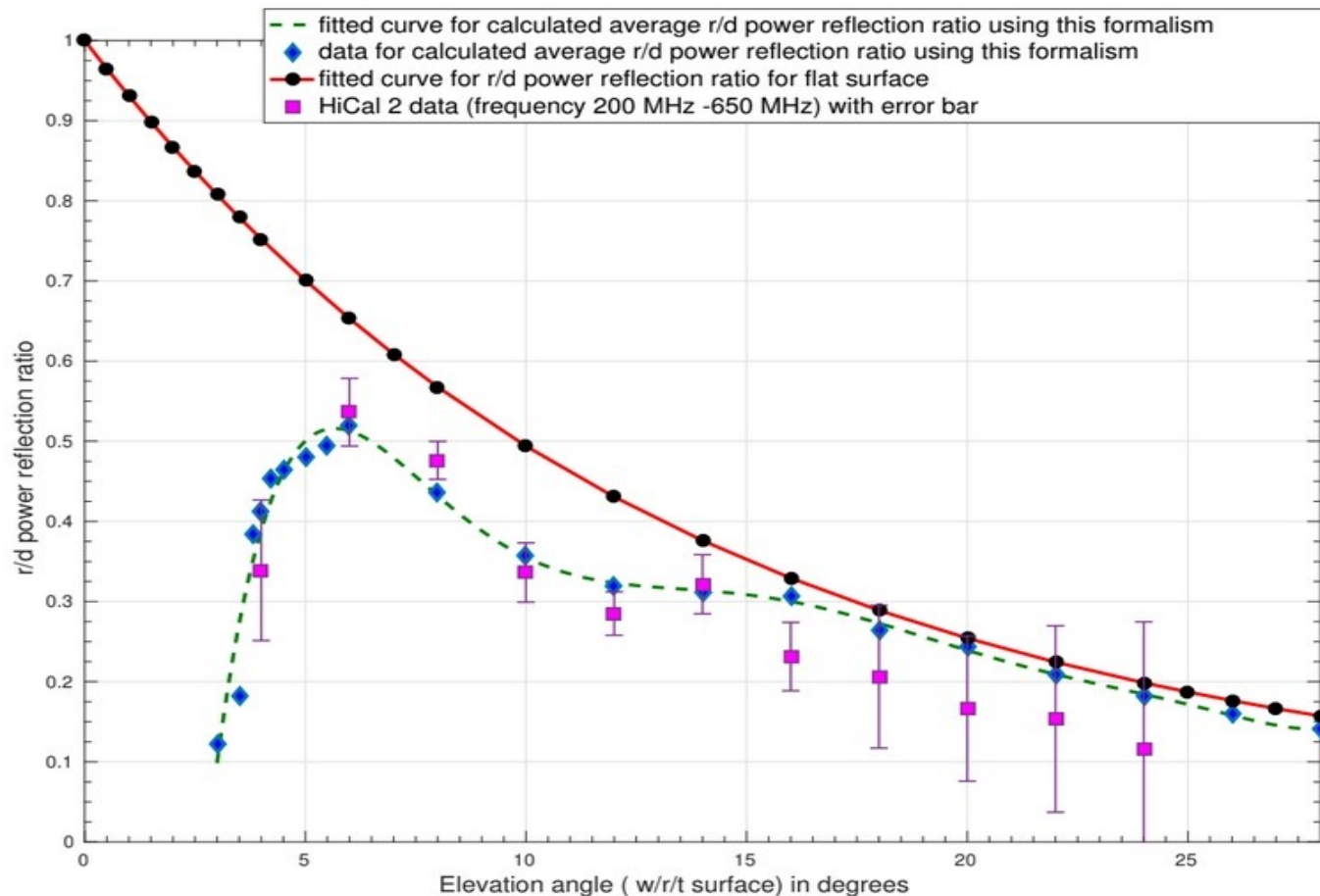
$$E_{r,y} = \frac{ik^3}{8\epsilon\pi^2} \tilde{\Pi}_{S,r} \left[f_r^{(s)} \cos^2 \tilde{\beta} - f_r^{(p)} \cos \tilde{\alpha} \cos(\tilde{\alpha} - 2\psi) \sin^2 \tilde{\beta} \right]$$

$$E_{(r,total),y} = \int_0^{2\pi} \int_0^{\frac{\pi}{2}-i\infty} F_{rough} E_{r,y} \sin \alpha d\alpha d\beta.$$

Take Ratio with the amplitude of Direct pulse propagated from Dipole to Detector

Compare this amplitude ratio r/d with the HiCal Experimental data

r/d power ratio for a spherical-rough surface: Local Plane Wave Approximation



P. Dasgupta and P Jain (Under Review: [Astroparticle Physics Journal](#)), arXiv:1811.00900v2

Using First Principle Calculation

We developed

**“First Complete Theoretical
Framework” for ANITA**

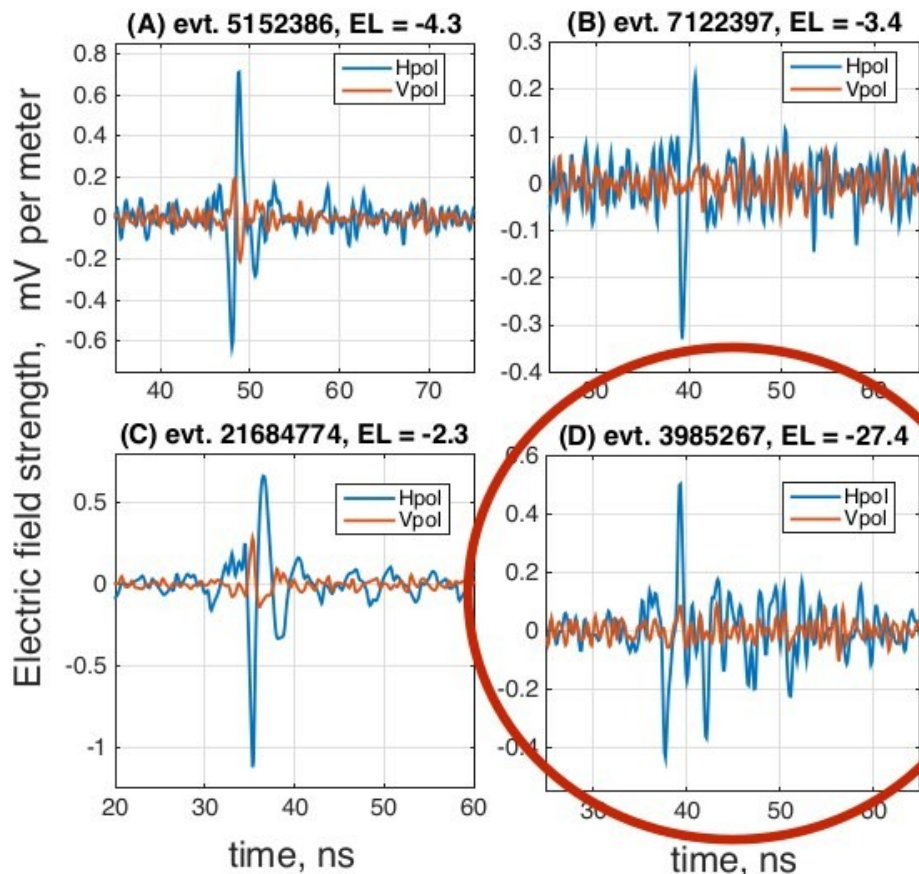
&

**its successor neutrino detection
experiments**

**“Anomalous Events”
Detected by
ANITA**

ANITA Anomalous Events

Two Unusual steeply pointed up-going air showers with $E \sim EeV$ scale



Dominantly H-Pol

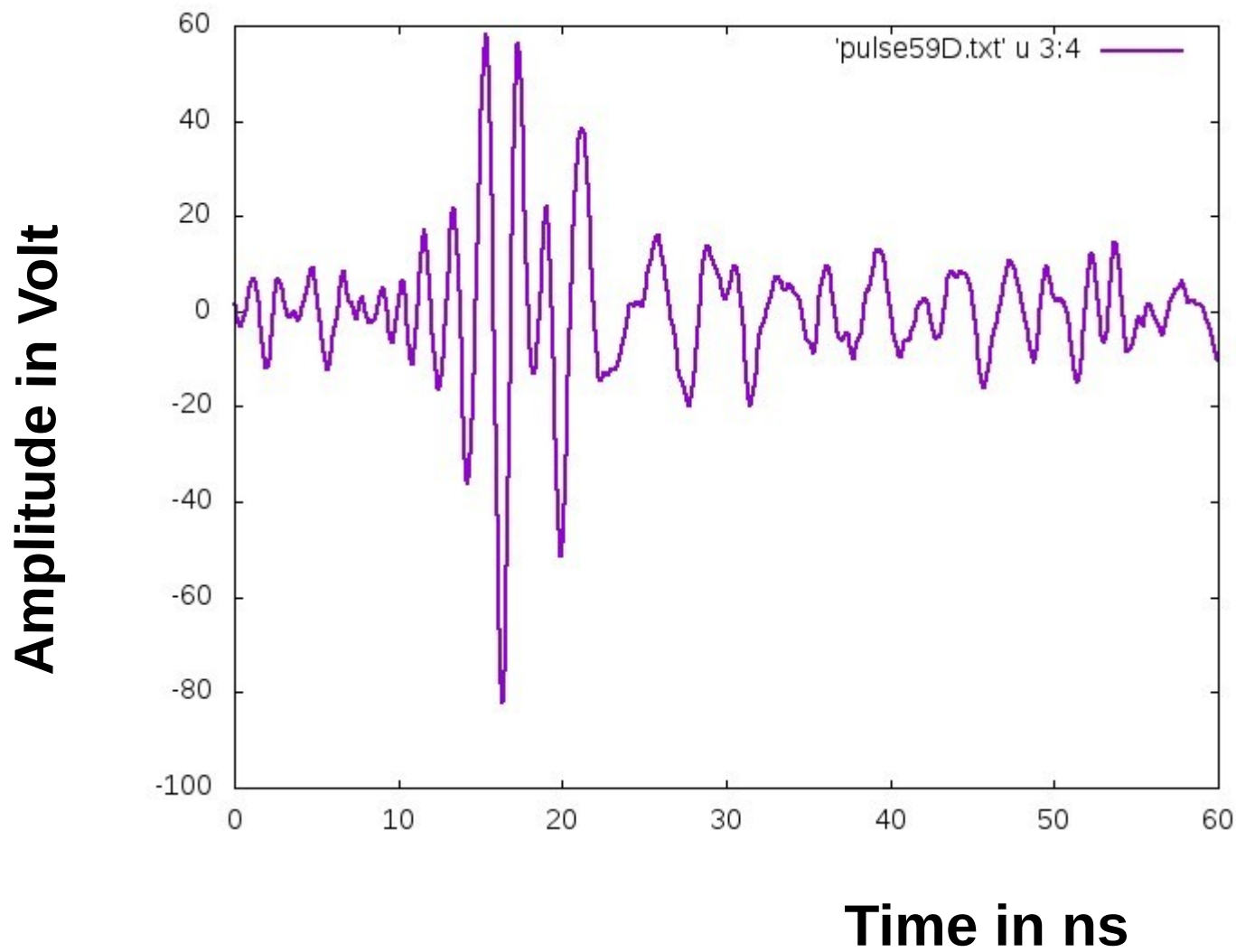
No Phase Inversion !

Tau-neutrino interaction in ice?

**Our Formalism Explain these
anomalous events??**

Next we try to unfold this mystery

HiCal Pulse



Generalizing Framework for Electromagnetic Pulses (Applicable to ANITA events)

- monochromatic spherical electromagnetic waves.
- Reflection from ice as a function of frequency, angle of reflection.

We need to consider Electromagnetic pulses to study the ANITA signals

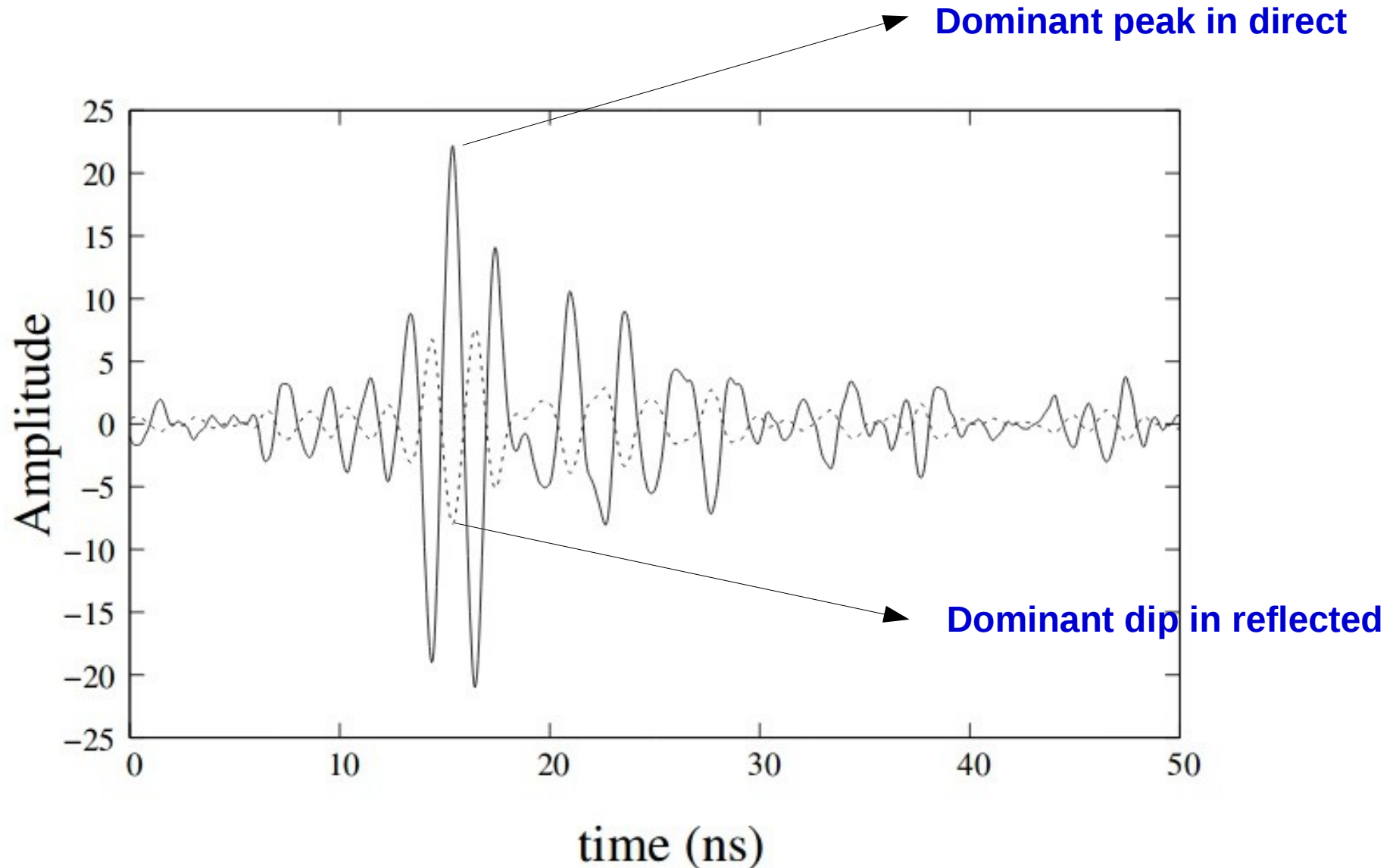
$$\tilde{F}(n) = \sum_{p=0}^{N-1} f(p) e^{i \frac{2\pi n}{N} p}$$

$$E'_{ref,y} = \int_0^{\frac{\pi}{2} - i\infty} \int_0^{2\pi} \int_{\omega} \frac{ik}{2\pi} \tilde{\Pi}_{S,r} F_{rough}(\omega, \alpha, \beta, \theta_z) \eta(\alpha, \beta, \omega) (\tilde{F}(\omega) e^{-i\omega(t+t_0)}) d\omega d\Omega.$$

Superposition of dipole radiation of different frequencies

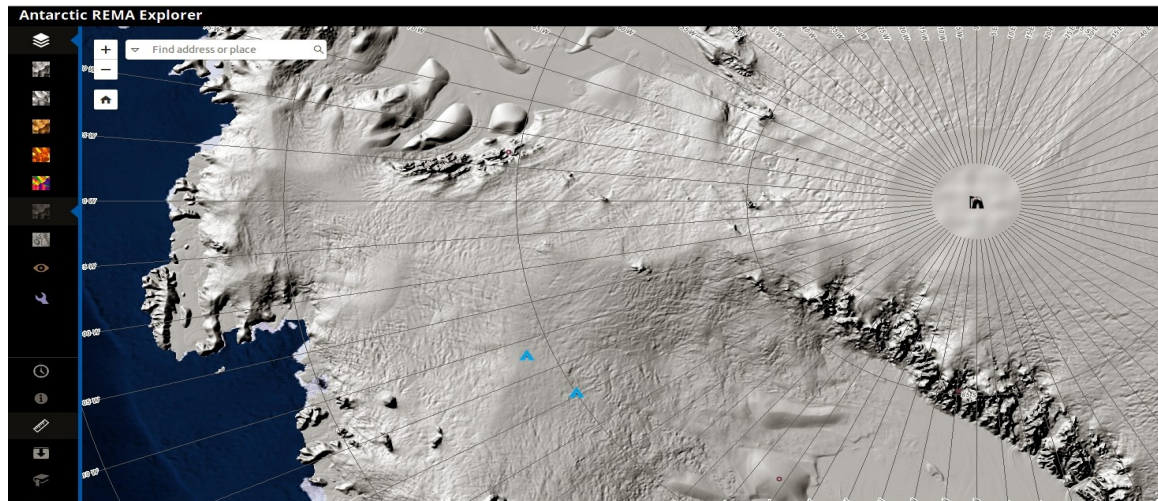
Incorporating our formalism to compute Direct and Reflected pulse profile (using HiCal 2 pulses)

Polarity of Reflected signals

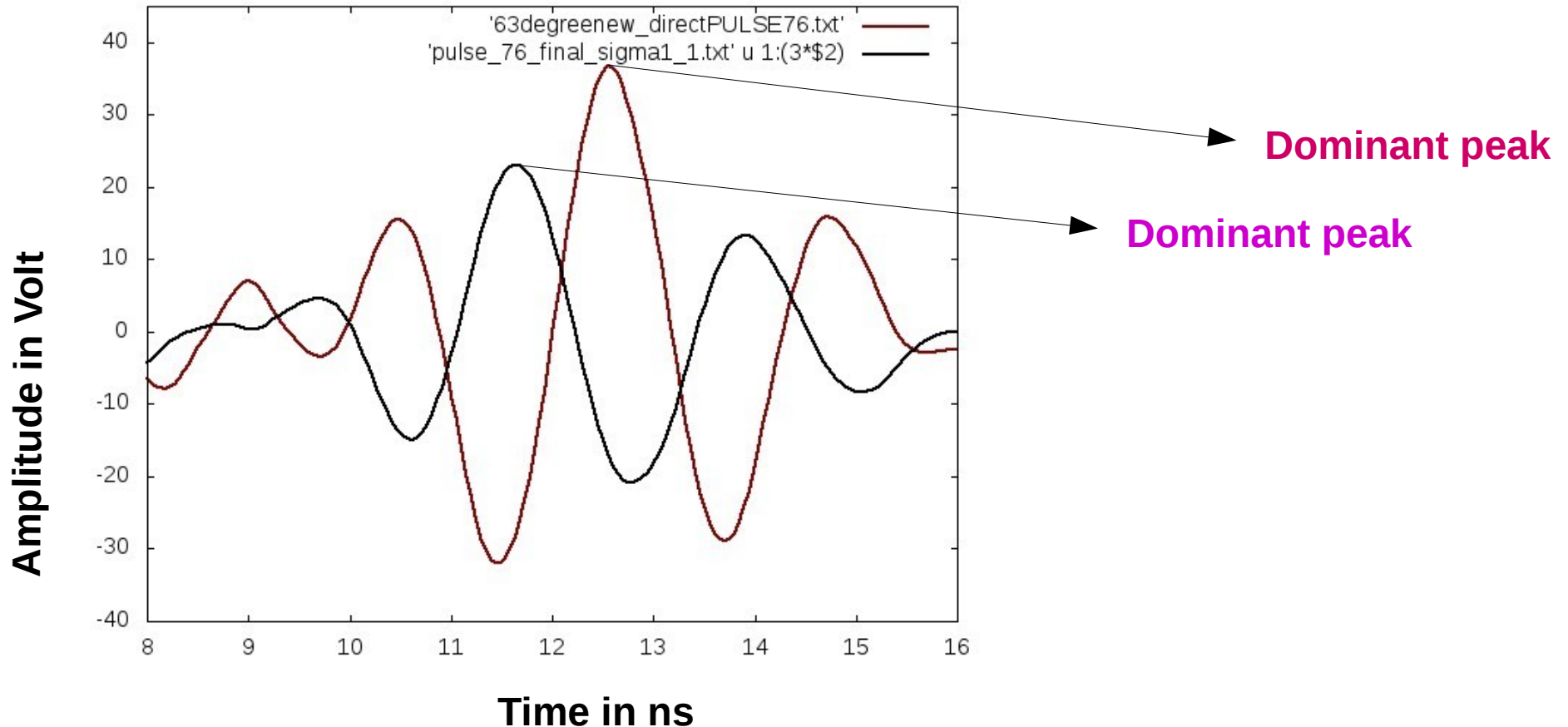


New Roughness Models

- **Antarctic topographic data** one side is quite smooth but the other side has lots of variation in altitude.
- **In order to account for this we allowed our incident angle to vary over a range of about 3 Km by about 1 degree.**
- **We also simply increase the curvature. This will model a hill like structure in the region of mystery events**

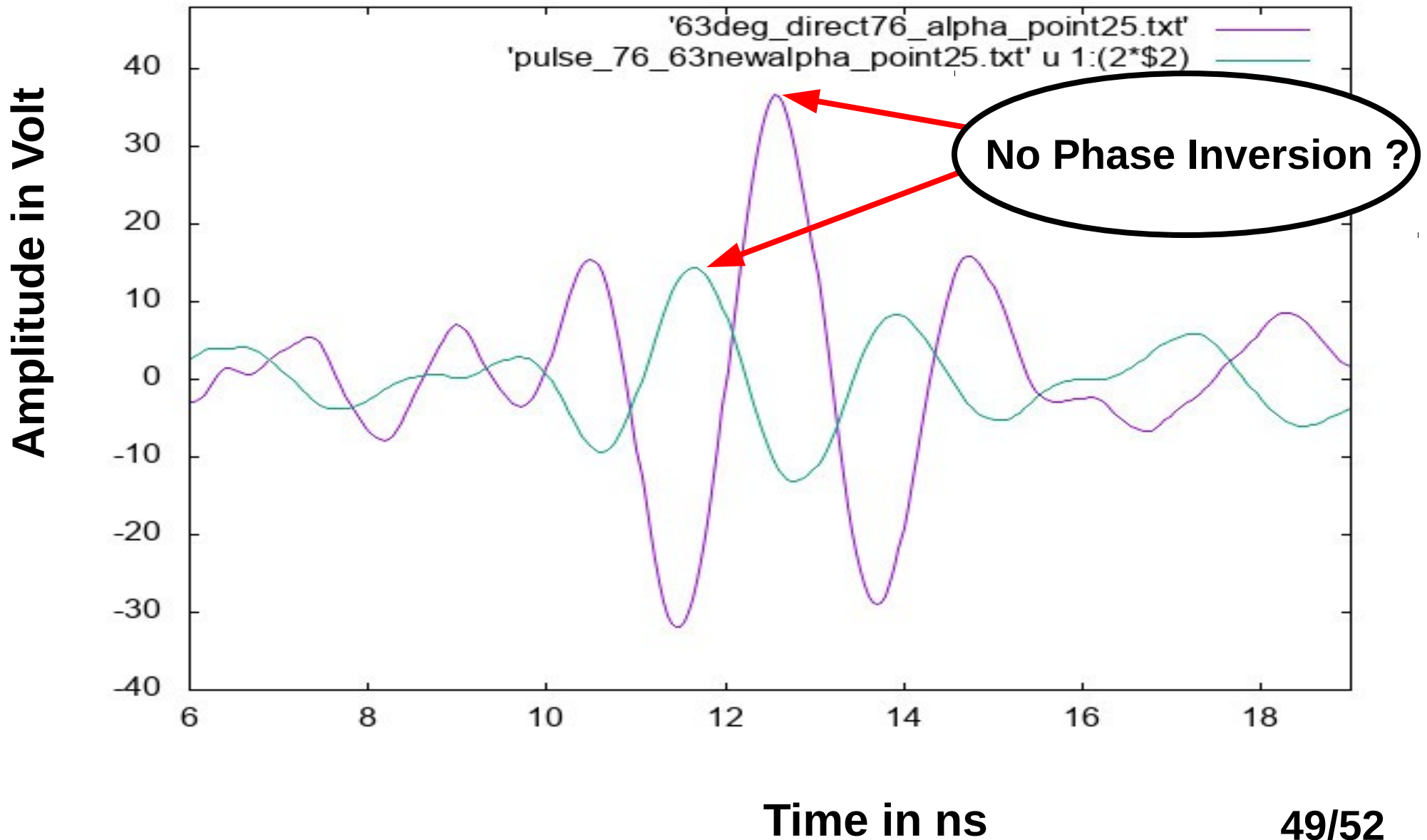


Non-Inversion of phase using new roughness model

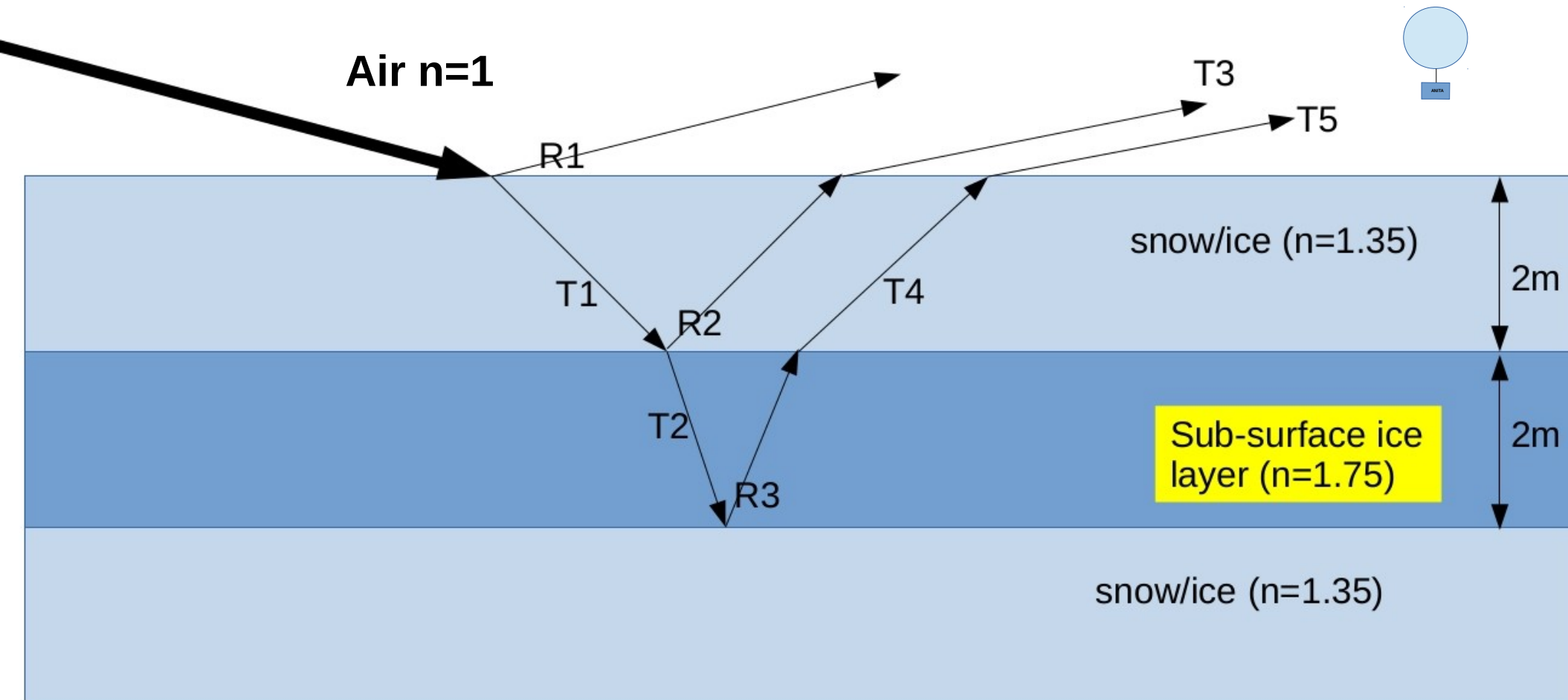


We see non-inversion of phase in simulated reflected pulses

Possible explanation for ANITA mystery events ?



Sub-Surface Reflection: Another Possible Explanation for Mystery Event



I am at the finishing stage of this work with **Prof. Dave Besson, PI of HiCal Expt** (work in progress)

Pic Courtesy: Dave Z Besson



Conclusion

We developed complete theoretical framework for UHECR induced radio detection at Balloon payload for a spherical, rough reflecting surface.

Future ground based and Balloon-borne Cosmic Ray detection experiments can use our formalism.

Incorporation of actual Antarctic surface topographical data in the ANITA Monte Carlo (icemc)

Explanation for ANITA mystery events ? We show that surface topography can cause additional phase inversion in pulses.

Our framework can be implemented for the in ice propagation of the radio signals applicable to RADAR, RNO-G project

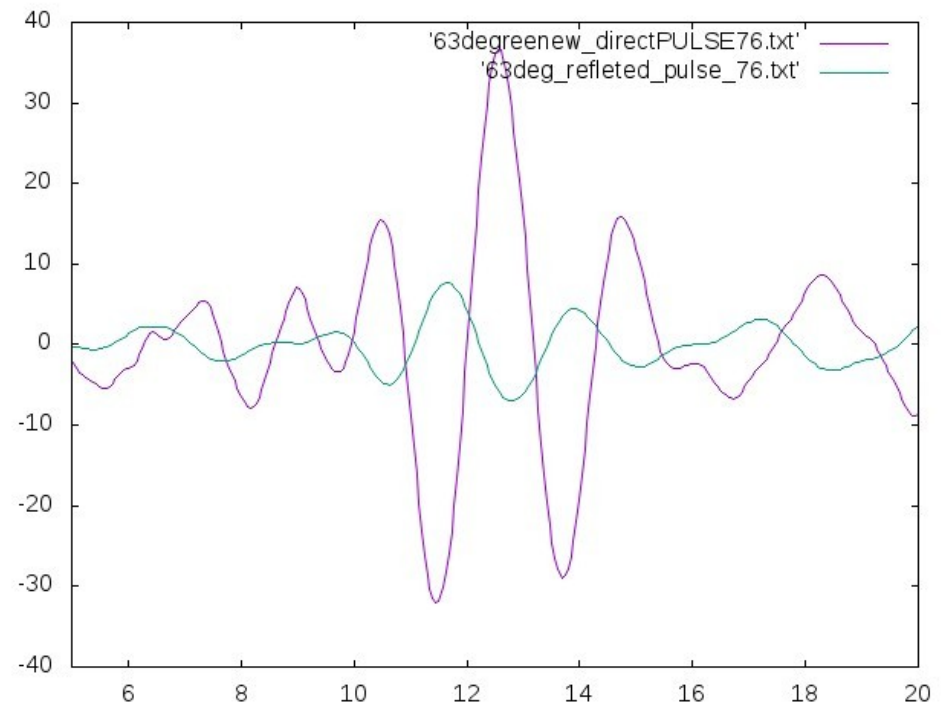
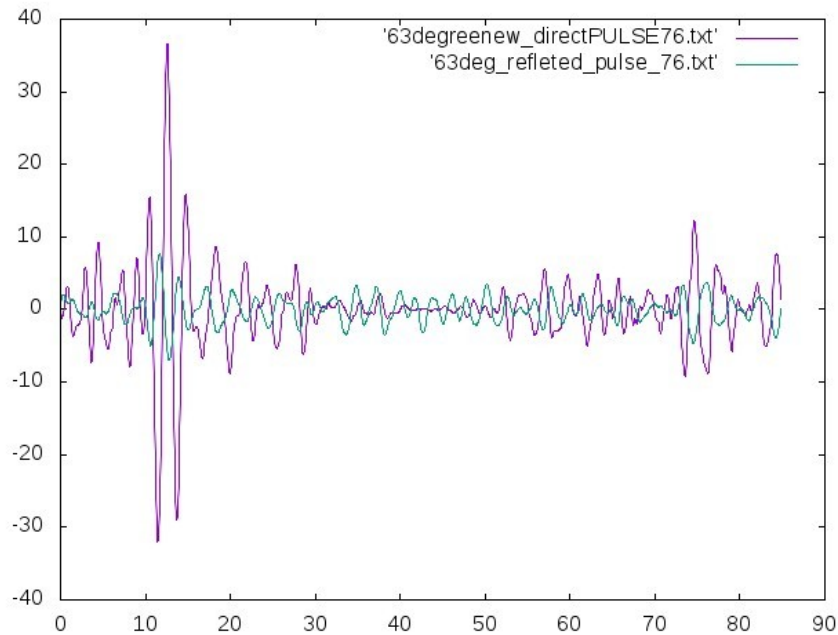
Thank You



BACK UP

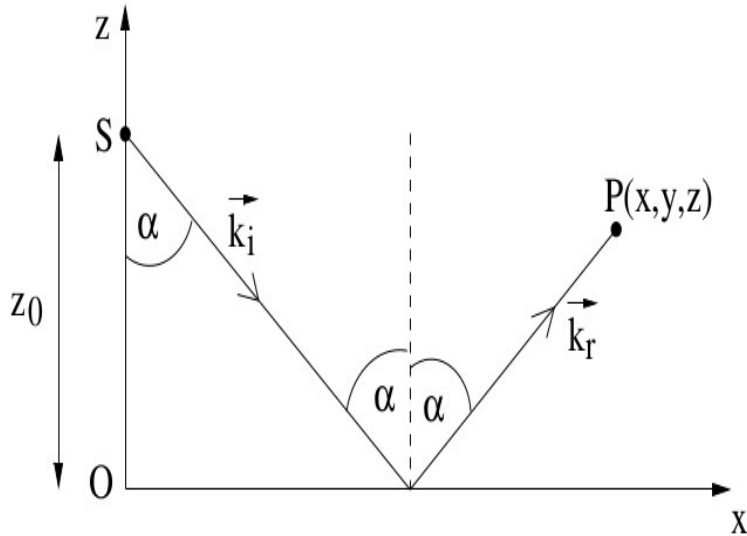
Recent results with random surface roughness

- **Random surface roughness profile**
- **No polarity Inversion !!**

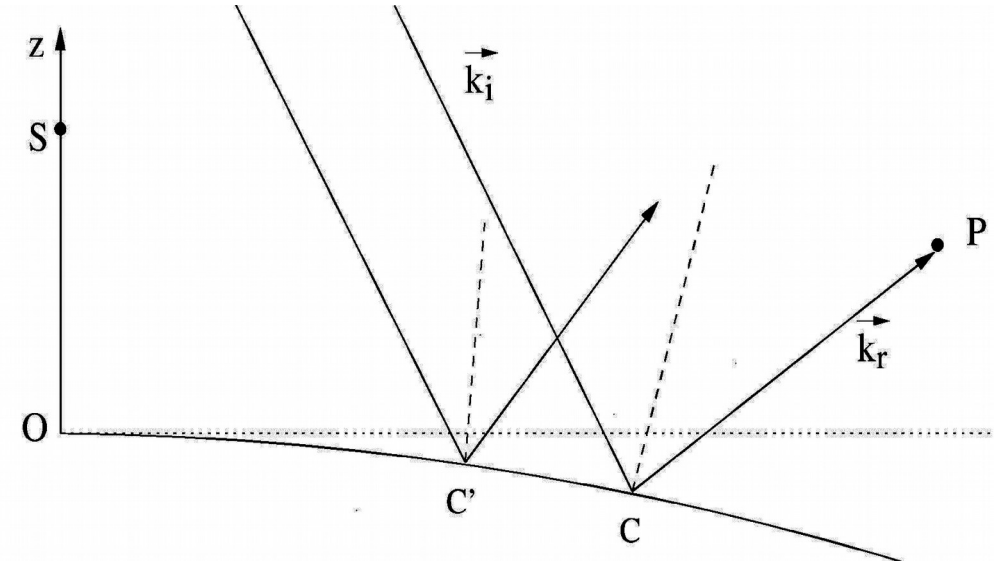


A Rigorous Framework for ANITA-HiCal

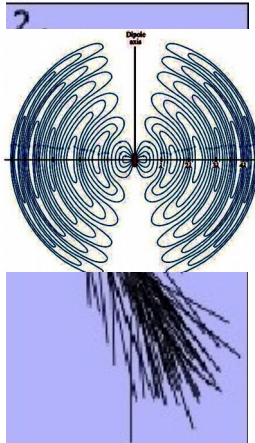
Reflection off a Flat Surface



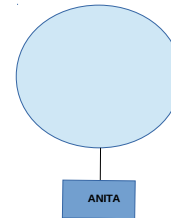
Reflection off a Spherical Surface



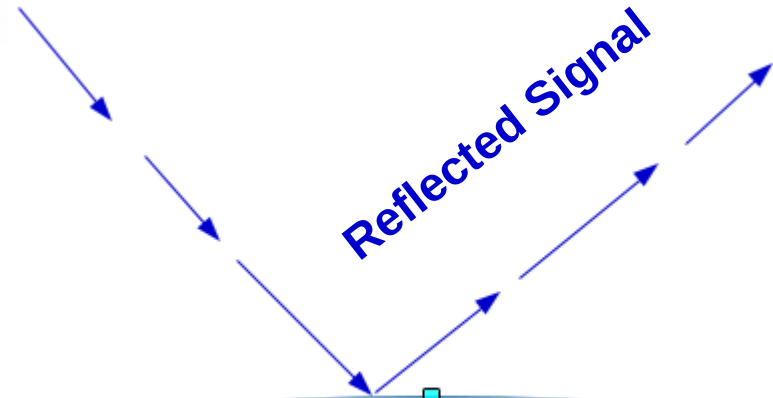
- A dipole radiator on the z axis



Direct Signal



Reflected Signal



- Extensive Air Shower (EAS)
- geosynchrotron radiation

Antarctic Ice Surface

Our formalism might be able to unfold the mystery of ANITA anomalous events.

We will submit these new results soon.

Future Scope in UHE Neutrino Study



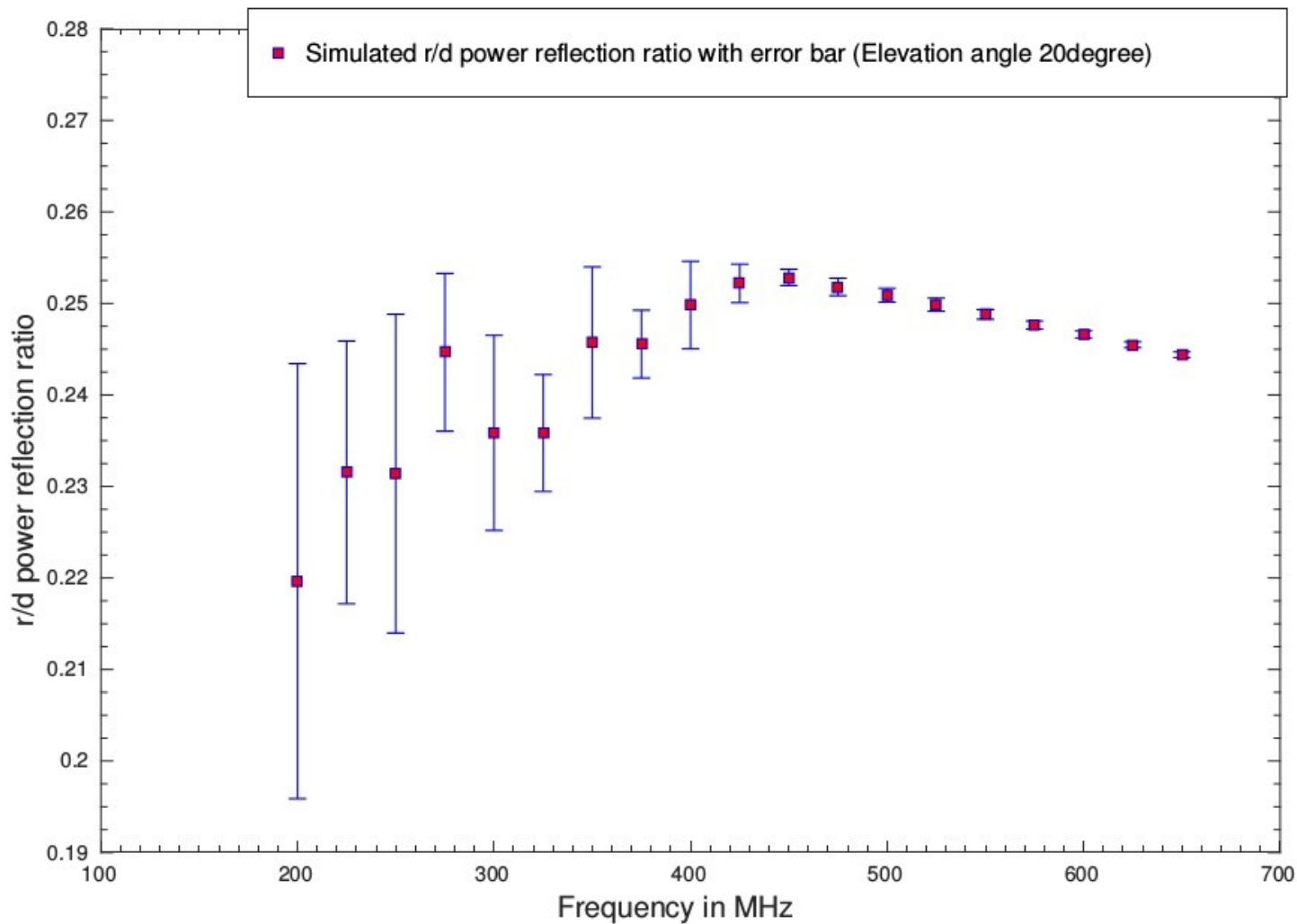
Huge ANITA Data to be analysed

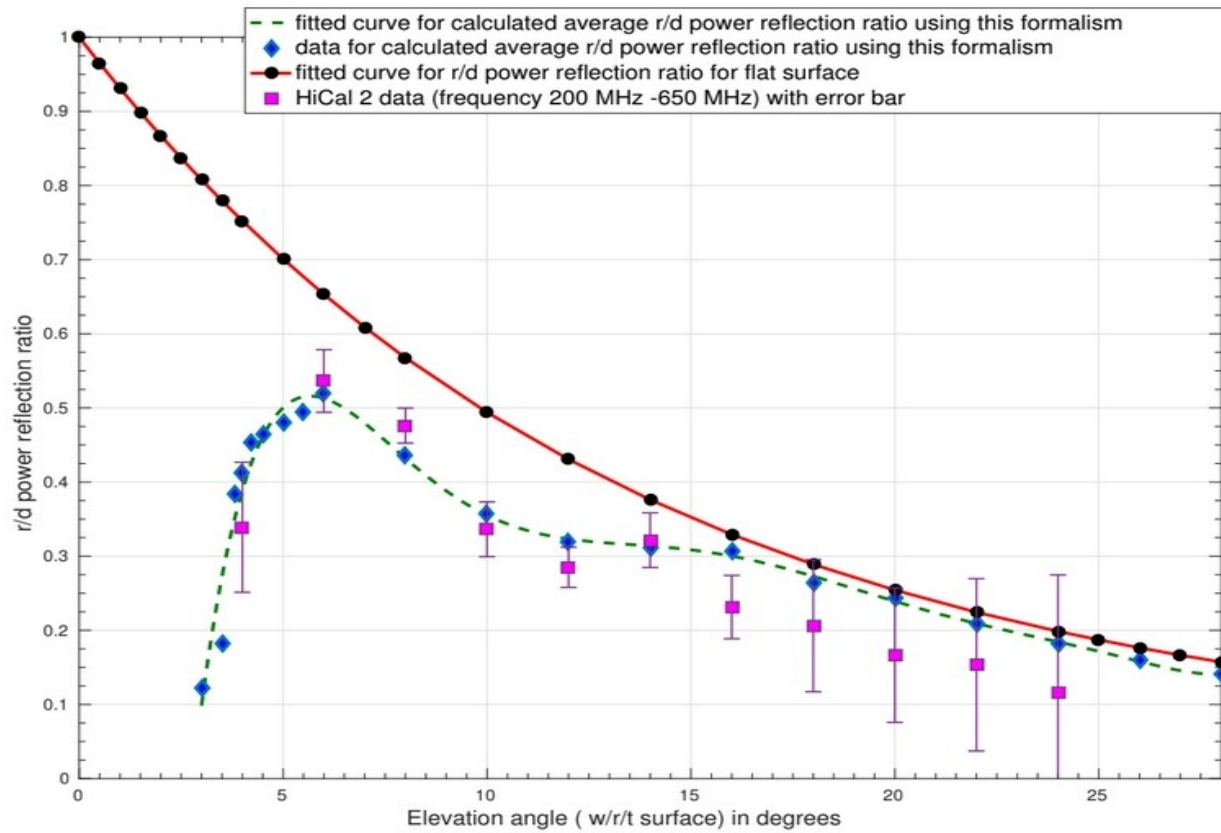
Cosmic Ray and Tau neutrino analysis

Unfolding Mystery events & the Sources

ANITA 5 Proposal !! ARA, ARIANA Experiment !

Frequency dependence of r/d power ratio

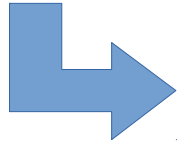




P. Dasgupta and P Jain arXiv:1811.00900, November 2018

For a Flat Surface

Reflected Field / Direct Field



Fresnel coefficients

Reflecting Surface is Curved

Reflection of Spherical waves from
Spherical-Rough surface

We also studied the case of non-uniform Roughness

Fourier-Bessel Integral: Expansion of Spherical Wave into plane waves

$$h_0^{(1)}(kR) = \frac{e^{ikR}}{ikR} = \int_{i\infty}^1 e^{ikR\eta} d\eta.$$

Using $k.R = k R \cos \gamma$

$$\frac{e^{ikR}}{ikR} = \int_0^{\frac{\pi}{2}-i\infty} e^{ikR \cos \gamma} \sin \gamma d\gamma$$

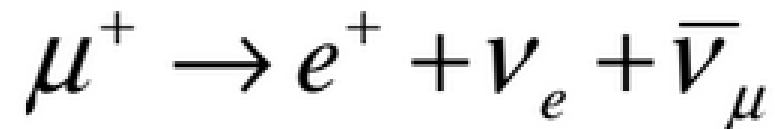
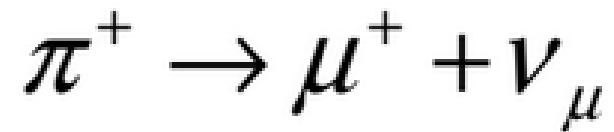
Since value of the integral is invariant to a rotation of the reference axes, Hence we get the desired Weyl representation of Spherical Waves into plane waves

$$\frac{e^{ikR}}{R} = \frac{ik}{2\pi} \int_0^{2\pi} \int_0^{\frac{\pi}{2}-i\infty} e^{ikR \cos \gamma} \sin \alpha d\alpha d\beta.$$

Why to study Ultra High Energy Neutrinos ??

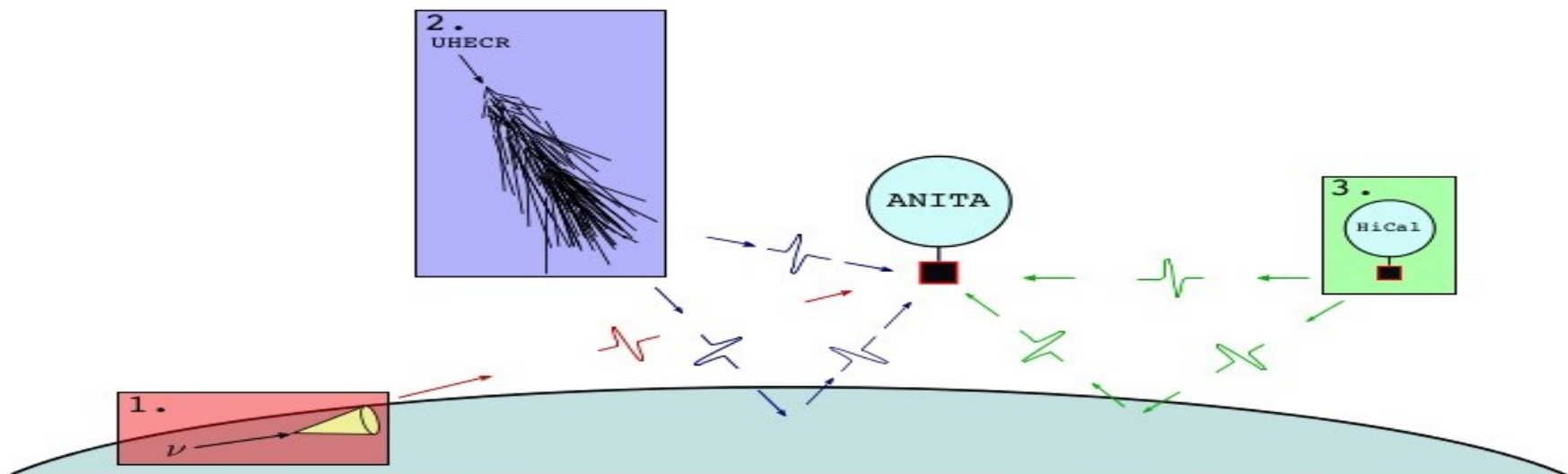


- **Ideal Astronomical Messengers**
- **Uncharged, not affected by B_{earth}**
- **New information on UHE ($> 10^{19}$ eV) CR**
- **GZK effect : CR interaction with Y_{CMB} produce neutrinos.**
- **UHE neutrino Sources !!**

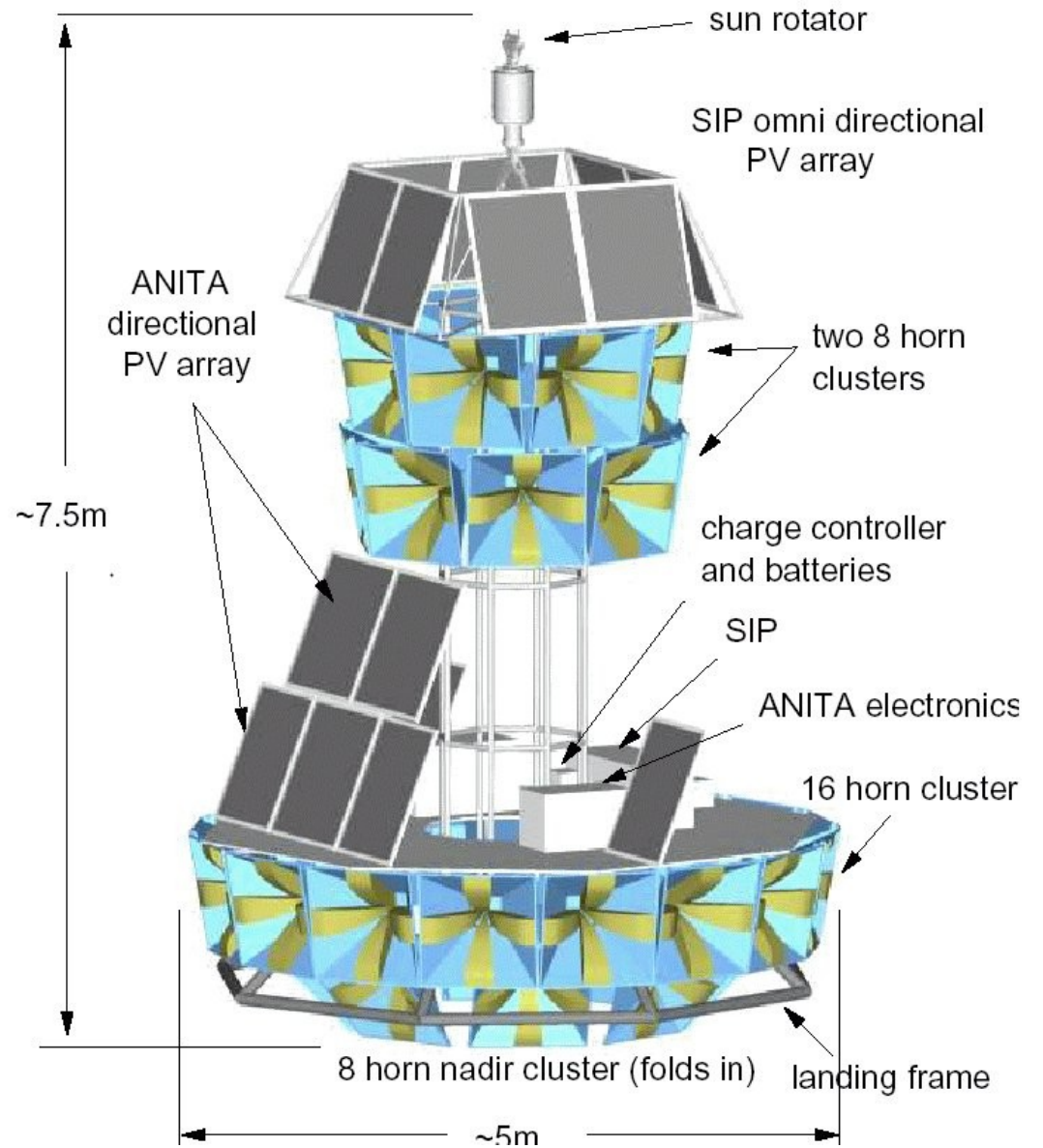
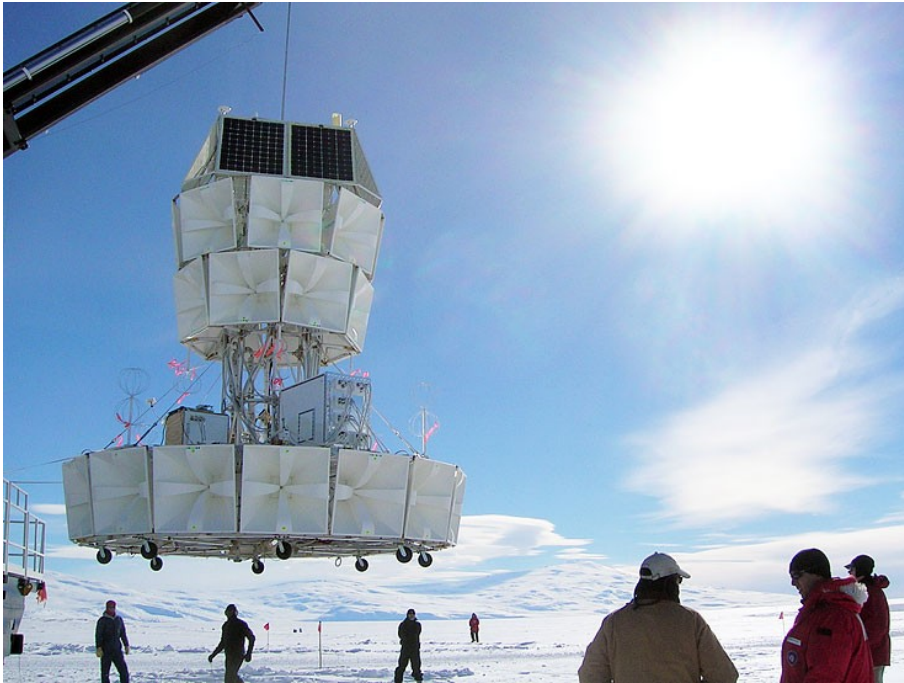


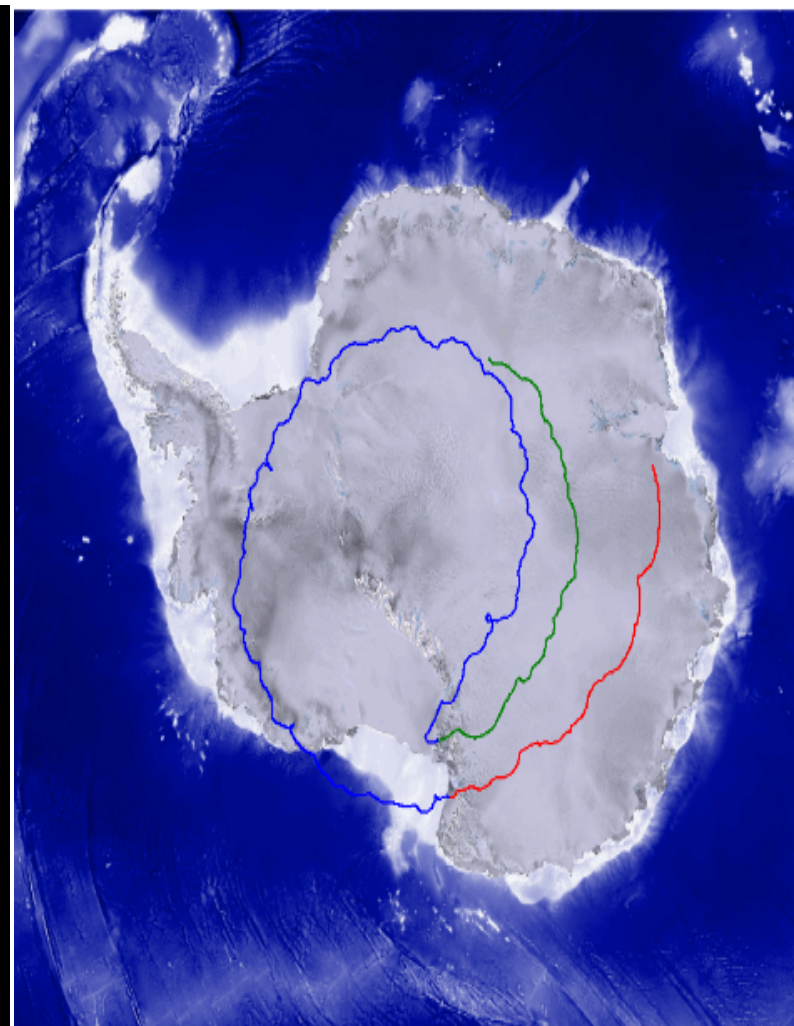
ANITA and HiCal Working Principle

- Antarctic Impulsive Transient Antenna is a balloon-borne RF (200-650) MHz Receiver Array.
- High Altitude Calibration (HiCal) is a Balloon-Borne RF Transmitter, in concert with the ANITA RF receiver array.
- ANITA-HiCal Measures Antarctic Surface Reflectivity in RF regime.
- Main Goal of ANITA is to detect Highest Energy Particles via the Radio signals produced by the UHECR interaction with Earth's atmosphere.
- Down Coming Charged Particles produce Mainly H-Pol radiation.



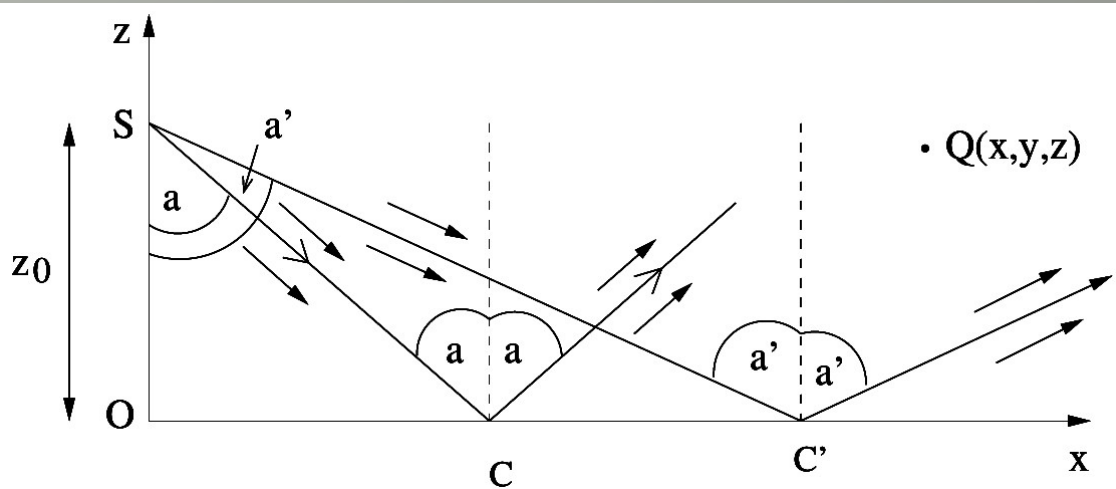
ANITA Detector





He balloon flying at a height 37Km above Antarctica, carries array of radio antennas to detect radio signals from Cosmic Neutrinos/UHECRs

Weyl Formalism : Decomposition of Spherical Waves into Plane Waves



Start with a Hertz dipole at $(0,0,z_0)$
 Hertz Potential (In Far Field $r \gg \lambda$)

$$\Pi_y(x, y, z) = \frac{e^{ikR}}{4\pi\epsilon R} + F_1(x, y, z)$$

Primary field Due to reflection

$$\vec{k}_I = k(\sin \alpha \cos \beta \hat{x} + \sin \alpha \sin \beta \hat{y} - \cos \alpha \hat{z})$$

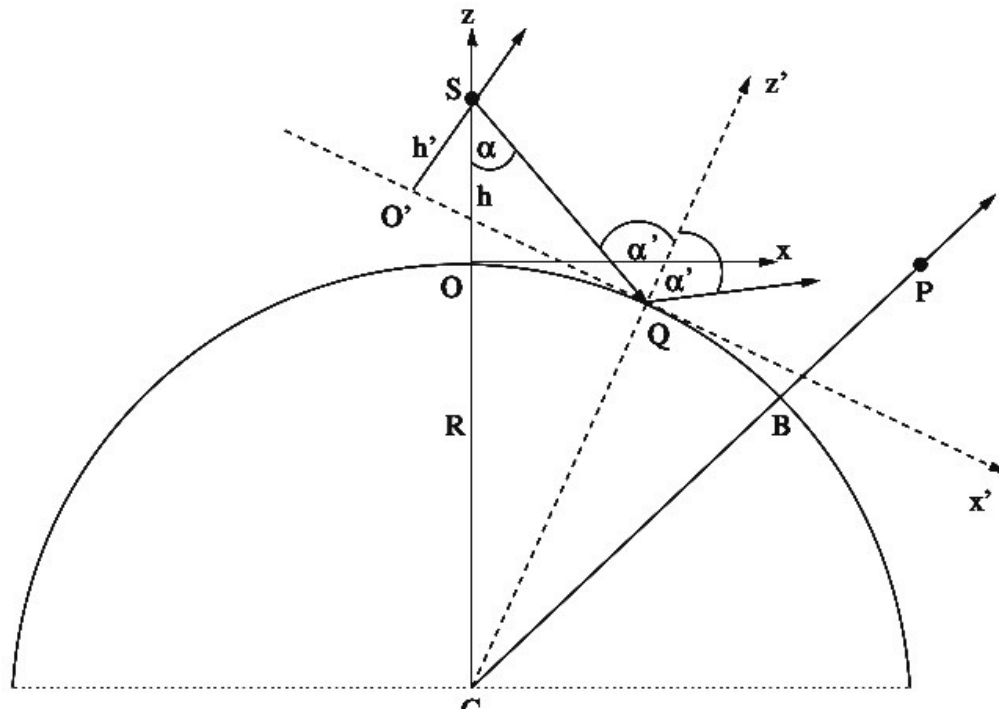
Incident wave vector $k(\alpha, \beta)$

$$\vec{k}_t = k_1[\sin \alpha_t \cos \beta_t \hat{x} + \sin \alpha_t \sin \beta_t \hat{y} - \cos \alpha_t \hat{z}]$$

Transmitted wave vector $k(\alpha_t, \beta_t)$

* Weyl Formalism (H. Weyl, Ann. Physik, 60,481,1919)
 Stratton(1941), Born & Wolf (1980)

Spherical Earth Surface: Reflection and Refraction of radio signals



$R_{\text{Earth}} \sim 6371 \text{ Km}$

Detector Height $z_0 \sim 37 \text{ Km}$

$$Rot = \begin{pmatrix} \cos(\alpha' - \alpha) \cos \beta & \cos(\alpha' - \alpha) \sin \beta & -\sin(\alpha' - \alpha) \\ -\sin \beta & \cos \beta & 0 \\ \sin(\alpha' - \alpha) \cos \beta & \sin(\alpha' - \alpha) \sin \beta & \cos(\alpha' - \alpha) \end{pmatrix}$$

S. Prohira, A. Novikov, P. Dasgupta, P. Jain et al. Phys. Rev. D 98, 042004

Include Non Uniform Roughness Parameter

Previously we incorporated Roughness Factor that assumed a circular region around the specular point

$$F(k, \rho, \theta) = \exp[-2k^2 \sigma_h(\rho_{\perp})^2 \cos^2 \theta_z] \quad \sigma_h(L) = \sigma_h(L_0) \left(\frac{L}{L_0} \right)^H$$

where, $\sigma_h(L_0) = 0.041$, $L_0 = 150$ m, $H = \text{Hurst Parameter} = 0.65$,

$$X^2 + Y^2 = L^2 \quad \longleftarrow \text{Circular}$$

Now, I use an elliptical region around the specular pt $X^2 + (aY)^2 = L^2$
with $a < 1$

We compute reflected pulses using this asymmetric roughness parameter "a"

choosing $a = 0.1, 0.25, 0.5$ and $a = 1$ (which is the symmetric case, as given by Peter Gorham's model)

$0.041 < \sigma_h(L_0) < 0.071$ and L_0 changed accordingly between 150m to 80 m

RESULTS with different asymmetric factors "a", and slightly changed $\sigma_h(L_0)$, and L_0 values are obtained.